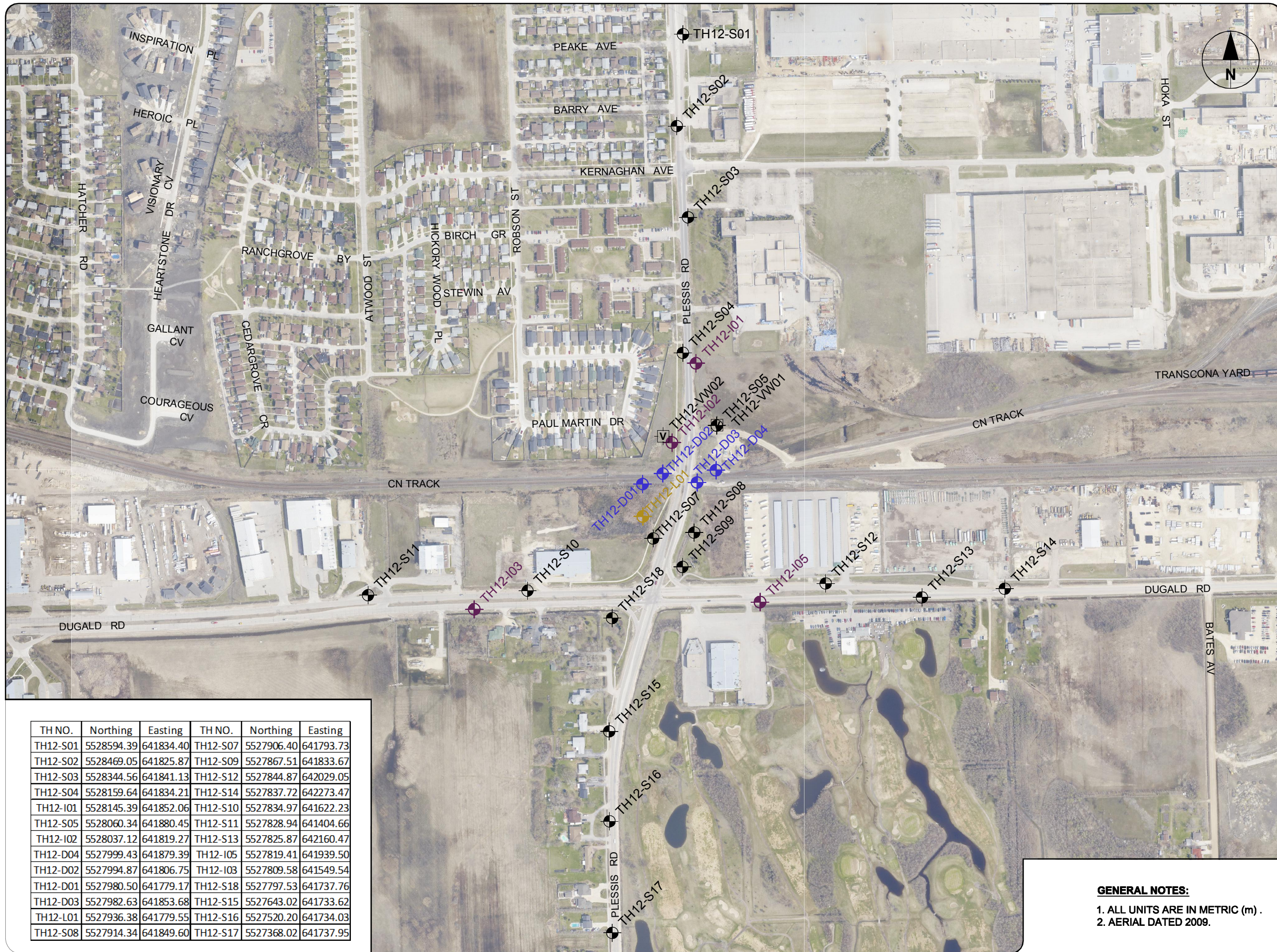


APPENDIX 'A'

GEOTECHNICAL REPORT

P:\16027304\1000-CADD\102-SHEETS\160273041-20-SHT-B-001_RX.dwg

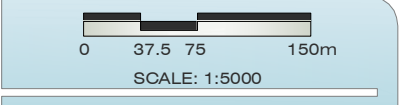


TEST HOLE LOCATION PLAN

- SHALLOW TEST HOLE
- INTERMEDIATE TEST HOLE
- DEEP TEST HOLE
- LIFT STATION TEST HOLE
- VIBRATING WIRE PIEZOMETER

TH NO.	Northing	Easting	TH NO.	Northing	Easting
TH12-S01	5528594.39	641834.40	TH12-S07	5527906.40	641793.73
TH12-S02	5528469.05	641825.87	TH12-S09	5527867.51	641833.67
TH12-S03	5528344.56	641841.13	TH12-S12	5527844.87	642029.05
TH12-S04	5528159.64	641834.21	TH12-S14	5527837.72	642273.47
TH12-I01	5528145.39	641852.06	TH12-S10	5527834.97	641622.23
TH12-S05	5528060.34	641880.45	TH12-S11	5527828.94	641404.66
TH12-I02	5528037.12	641819.27	TH12-S13	5527825.87	642160.47
TH12-D04	5527999.43	641879.39	TH12-I05	5527819.41	641939.50
TH12-D02	5527994.87	641806.75	TH12-I03	5527809.58	641549.54
TH12-D01	5527980.50	641779.17	TH12-S18	5527797.53	641737.76
TH12-D03	5527982.63	641853.68	TH12-S15	5527643.02	641733.62
TH12-L01	5527936.38	641779.55	TH12-S16	5527520.20	641734.03
TH12-S08	5527914.34	641849.60	TH12-S17	5527368.02	641737.95

GENERAL NOTES:
 1. ALL UNITS ARE IN METRIC (m) .
 2. AERIAL DATED 2009.



AECOM Canada Ltd.

GENERAL STATEMENT

NORMAL VARIABILITY OF SUBSURFACE CONDITIONS

The scope of the investigation presented herein is limited to an investigation of the subsurface conditions as to suitability for the proposed project. This report has been prepared to aid in the evaluation of the site and to assist the engineer in the design of the facilities. Our description of the project represents our understanding of the significant aspects of the project relevant to the design and construction of earth work, foundations and similar. In the event of any changes in the basic design or location of the structures as outlined in this report or plan, we should be given the opportunity to review the changes and to modify or reaffirm in writing the conclusions and recommendations of this report.

The analysis and recommendations presented in this report are based on the data obtained from the borings and test pit excavations made at the locations indicated on the site plans and from other information discussed herein. This report is based on the assumption that the subsurface conditions everywhere are not significantly different from those disclosed by the borings and excavations. However, variations in soil conditions may exist between the excavations and, also, general groundwater levels and conditions may fluctuate from time to time. The nature and extent of the variations may not become evident until construction. If subsurface conditions differ from those encountered in the exploratory borings and excavations, are observed or encountered during construction, or appear to be present beneath or beyond excavations, we should be advised at once so that we can observe and review these conditions and reconsider our recommendations where necessary.

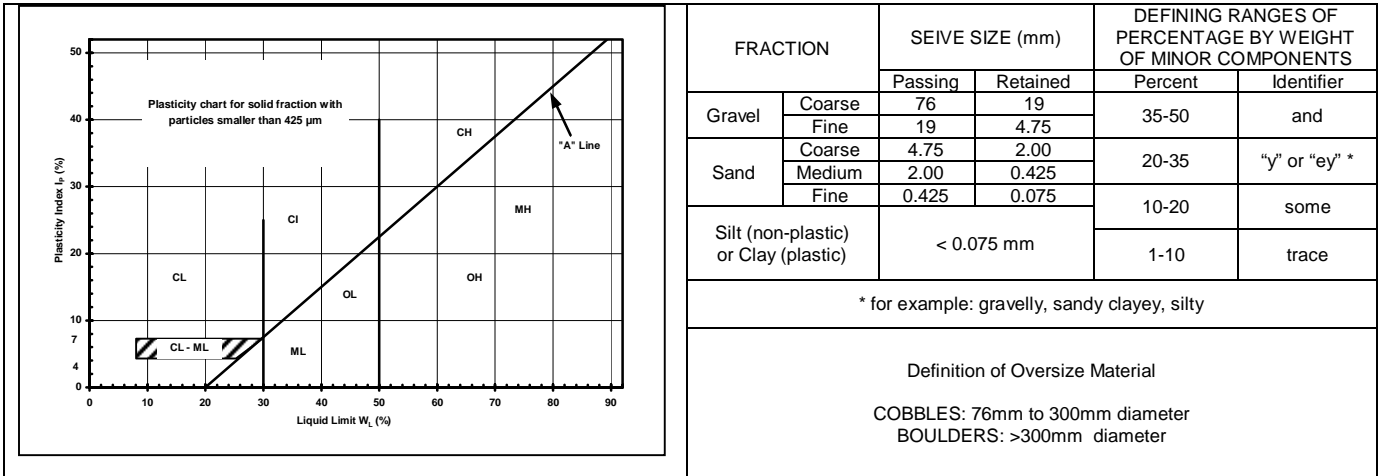
Since it is possible for conditions to vary from those assumed in the analysis and upon which our conclusions and recommendations are based, a contingency fund should be included in the construction budget to allow for the possibility of variations which may result in modification of the design and construction procedures.

In order to observe compliance with the design concepts, specifications or recommendations and to allow design changes in the event that subsurface conditions differ from those anticipated, we recommend that all construction operations dealing with earth work and the foundations be observed by an experienced soils engineer. We can be retained to provide these services for you during construction. In addition, we can be retained to review the plans and specifications that have been prepared to check for substantial conformance with the conclusions and recommendations contained in our report.

EXPLANATION OF FIELD & LABORATORY TEST DATA

Description			AECOM Log Symbols	USCS Classification	Laboratory Classification Criteria				
					Fines (%)	Grading	Plasticity	Notes	
COARSE GRAINED SOILS	GRAVELS (More than 50% of coarse fraction of gravel size)	CLEAN GRAVELS (Little or no fines)	Well graded gravels, sandy gravels, with little or no fines		GW	0-5	$C_u > 4$ $1 < C_c < 3$	Dual symbols if 5-12% fines. Dual symbols if above "A" line and $4 < W_p < 7$ $C_u = \frac{D_{60}}{D_{10}}$ $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$	
			Poorly graded gravels, sandy gravels, with little or no fines		GP	0-5	Not satisfying GW requirements		
		DIRTY GRAVELS (With some fines)	Silty gravels, silty sandy gravels		GM	> 12			Atterberg limits below "A" line or $W_p < 4$
			Clayey gravels, clayey sandy gravels		GC	> 12			Atterberg limits above "A" line or $W_p < 7$
	SANDS (More than 50% of coarse fraction of sand size)	CLEAN SANDS (Little or no fines)	Well graded sands, gravelly sands, with little or no fines		SW	0-5	$C_u > 6$ $1 < C_c < 3$		
			Poorly graded sands, gravelly sands, with little or no fines		SP	0-5	Not satisfying SW requirements		
		DIRTY SANDS (With some fines)	Silty sands, sand-silt mixtures		SM	> 12			Atterberg limits below "A" line or $W_p < 4$
			Clayey sands, sand-clay mixtures		SC	> 12			Atterberg limits above "A" line or $W_p < 7$
FINE GRAINED SOILS	SILTS (Below 'A' line negligible organic content)	$W_L < 50$	Inorganic silts, silty or clayey fine sands, with slight plasticity		ML		Classification is Based upon Plasticity Chart		
		$W_L > 50$	Inorganic silts of high plasticity		MH				
	CLAYS (Above 'A' line negligible organic content)	$W_L < 30$	Inorganic clays, silty clays, sandy clays of low plasticity, lean clays		CL				
		$30 < W_L < 50$	Inorganic clays and silty clays of medium plasticity		CI				
		$W_L > 50$	Inorganic clays of high plasticity, fat clays		CH				
	ORGANIC SILTS & CLAYS (Below 'A' line)	$W_L < 50$	Organic silts and organic silty clays of low plasticity		OL				
		$W_L > 50$	Organic clays of high plasticity		OH				
	HIGHLY ORGANIC SOILS		Peat and other highly organic soils		Pt	Von Post Classification Limit		Strong colour or odour, and often fibrous texture	
	Asphalt		Till			AECOM			
	Concrete		Bedrock (Undifferentiated)						
	Fill		Bedrock (Limestone)						

When the above classification terms are used in this report or test hole logs, the designated fractions may be visually estimated and not measured.



LEGEND OF SYMBOLS

Laboratory and field tests are identified as follows:

- q_u - undrained shear strength (kPa) derived from unconfined compression testing.
- T_v - undrained shear strength (kPa) measured using a torvane
- pp - undrained shear strength (kPa) measured using a pocket penetrometer.
- L_v - undrained shear strength (kPa) measured using a lab vane.
- F_v - undrained shear strength (kPa) measured using a field vane.
- γ - bulk unit weight (kN/m^3).
- SPT - Standard Penetration Test. Recorded as number of blows (N) from a 63.5 kg hammer dropped 0.76 m (free fall) which is required to drive a 51 mm O.D. Raymond type sampler 0.30 m into the soil.
- DPPT - Drive Point Pentrometer Test. Recorded as number of blows from a 63.5 kg hammer dropped 0.76 m (free fall) which is required to drive a 50 mm drive point 0.30 m into the soil.
- w - moisture content (W_L , W_P)

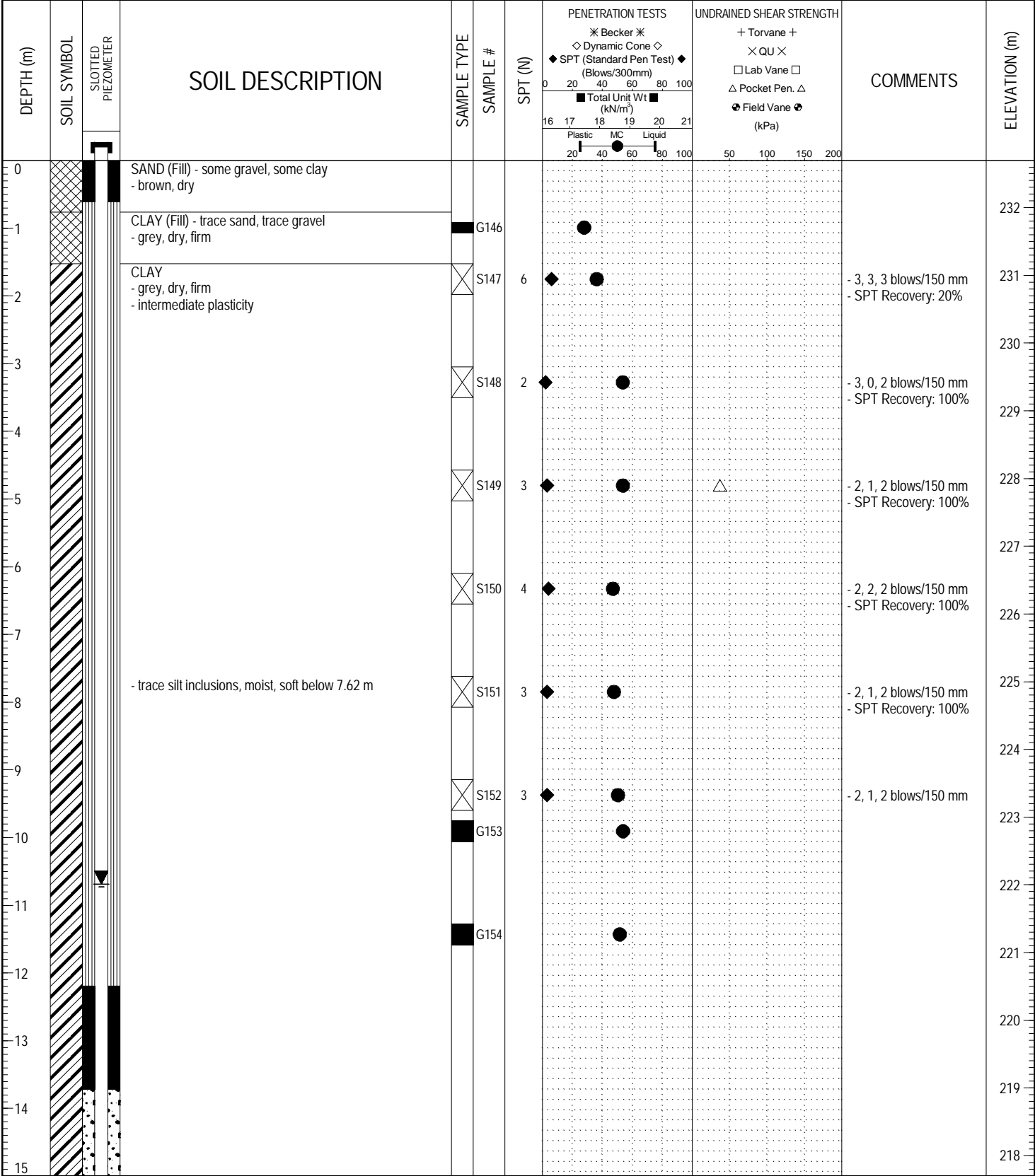
The undrained shear strength (S_u) of a cohesive soil can be related to its consistency as follows:

S_u (kPa)	CONSISTENCY
<12	very soft
12 – 25	soft
25 – 50	medium or firm
50 – 100	stiff
100 – 200	very stiff
200	hard

The resistance (N) of a non-cohesive soil can be related to compactness condition as follows

N – BLOWS/0.30 m	COMPACTNESS
0 - 4	very loose
4 - 10	loose
10 - 30	compact
30 - 50	dense
50	very dense

PROJECT: Plessis Road Underpass		CLIENT: City of Winnipeg		TESTHOLE NO: TH12-D01		
LOCATION: Plessis South Bound/CN Rail Intersection, West Shoulder Lawn		METHOD: Mobile B-40, 125 mm SSA		PROJECT NO.: 60273041		
CONTRACTOR: Maple Leaf Drilling Ltd.		METHOD: Mobile B-40, 125 mm SSA		ELEVATION (m): 232.70		
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
BACKFILL TYPE	BENTONITE	GRAVEL	SLOUGH	GROUT	CUTTINGS	SAND

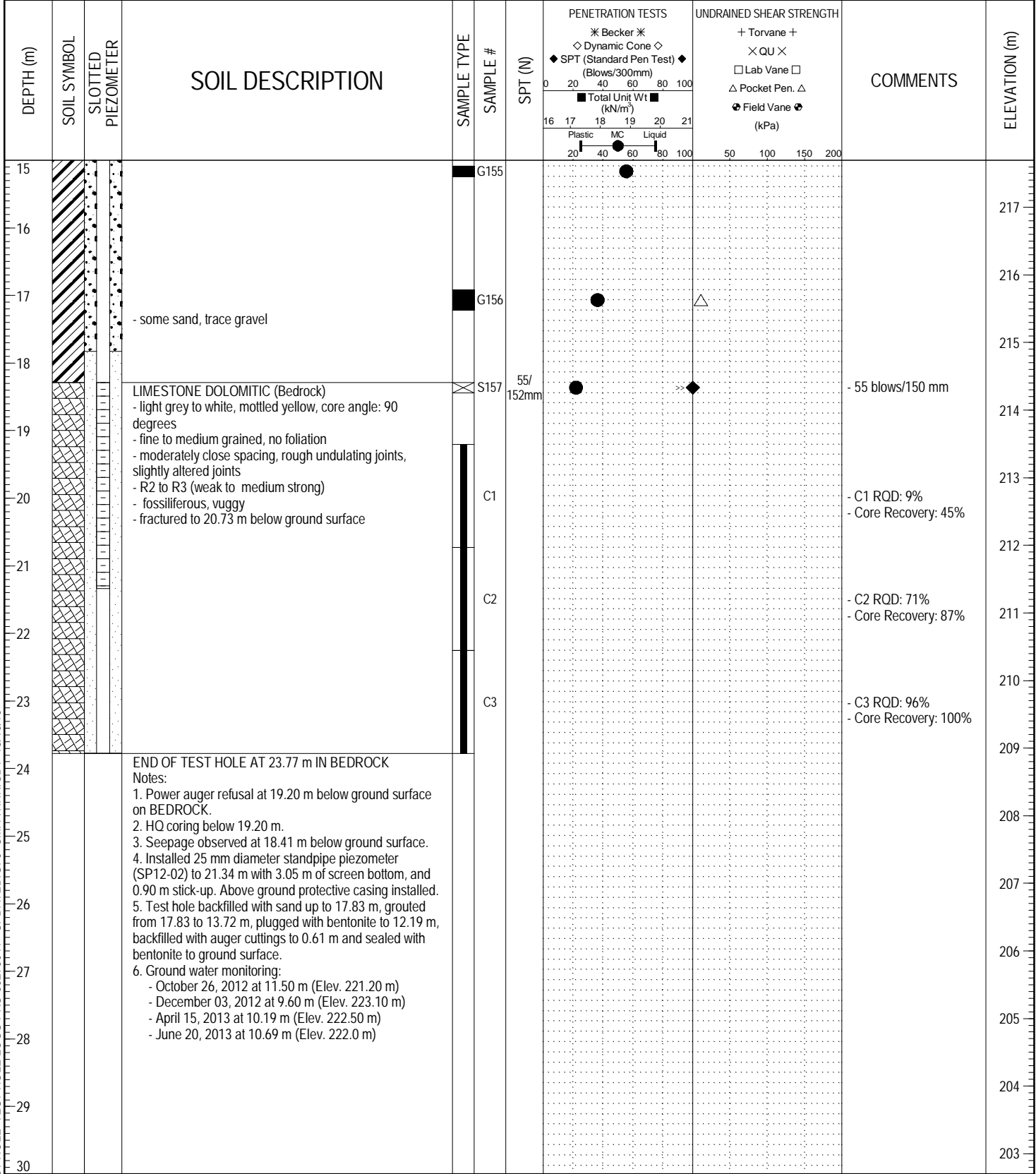


LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 23.77 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/26
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 2

PROJECT: Plessis Road Underpass		CLIENT: City of Winnipeg		TESTHOLE NO: TH12-D01		
LOCATION: Plessis South Bound/CN Rail Intersection, West Shoulder Lawn		METHOD: Mobile B-40, 125 mm SSA		PROJECT NO.: 60273041		
CONTRACTOR: Maple Leaf Drilling Ltd.		METHOD: Mobile B-40, 125 mm SSA		ELEVATION (m): 232.70		
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
BACKFILL TYPE	BENTONITE	GRAVEL	SLOUGH	GROUT	CUTTINGS	SAND



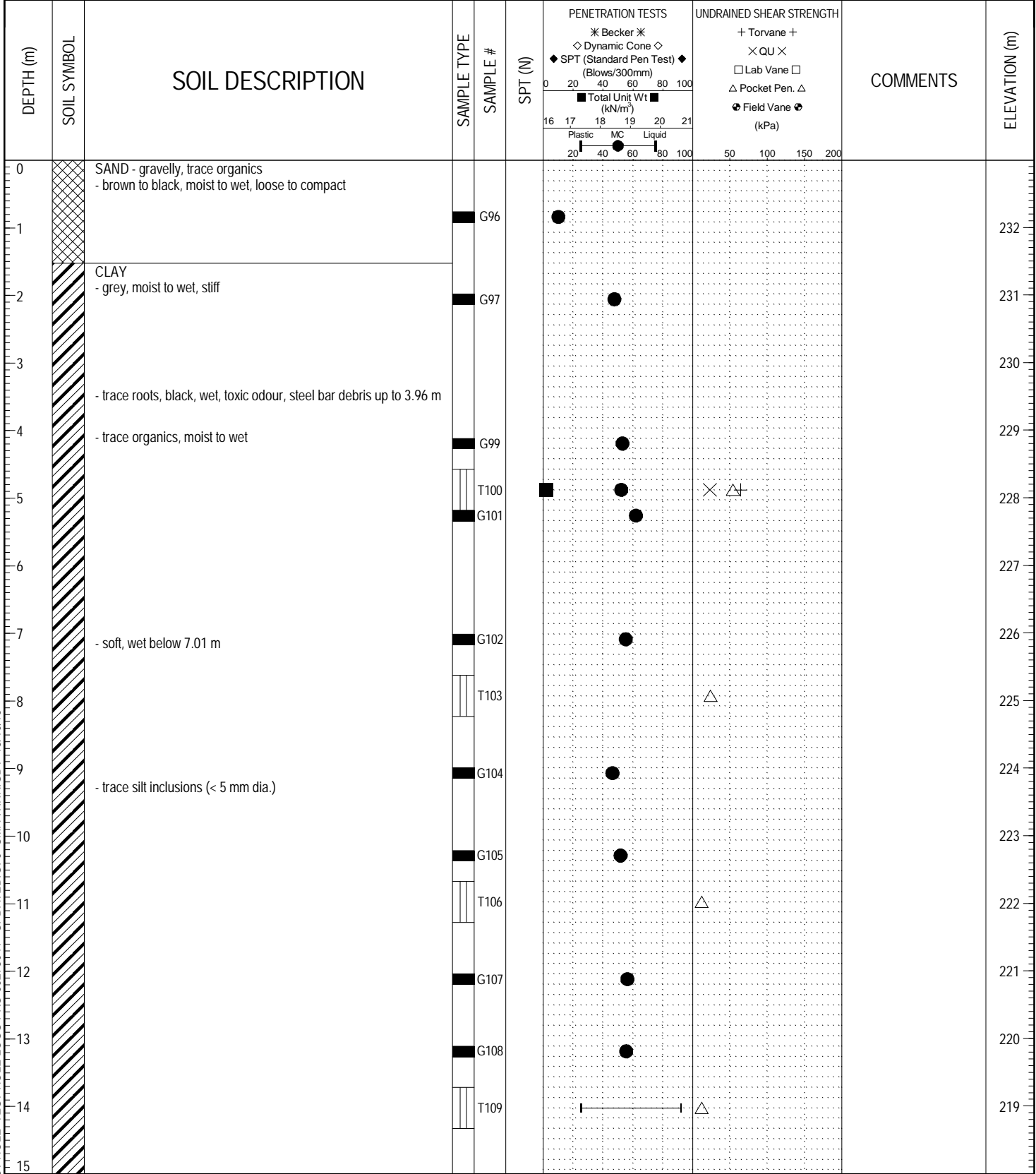
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 23.77 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/26
PROJECT ENGINEER: Zeyad Shukri	Page 2 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-D02
LOCATION: Plessis South Bound/CN Rail Intersection, West Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Mobile B-40, 125 mm SSA	ELEVATION (m): 232.99

SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
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LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 21.95 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/22
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-D02
LOCATION: Plessis South Bound/CN Rail Intersection, West Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Mobile B-40, 125 mm SSA	ELEVATION (m): 232.99

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION (m)
						Becker	Dynamic Cone	Torvane	QU		
15											
16				G110							217
17				G111							216
18				G112							215
19		LIMESTONE (Bedrock) - light grey to white, core angle: 90 degrees - fine to medium grained, no foliation - close spacing, rough undulating joints, slightly altered joints - R2 to R3 (weak to medium strong) - fossiliferous, filled vugs - high calcium limestone		C1						- C1 ROD: 26% - Core Recovery: 66%	214
20				C2						- C2 ROD: 72% - Core Recovery: 100%	213
21											
22		END OF TEST HOLE AT 21.95 m IN BEDROCK Notes: 1. Power auger refusal at 18.90 m below ground surface on BEDROCK. 2. HQ coring below 18.90 m. 3. Test hole grouted up to 13.72 m, plugged with bentonite from 13.72 to 12.80 m and backfilled with auger cuttings to ground surface.									211
23											210
24											209
25											208
26											207
27											206
28											205
29											204
30											

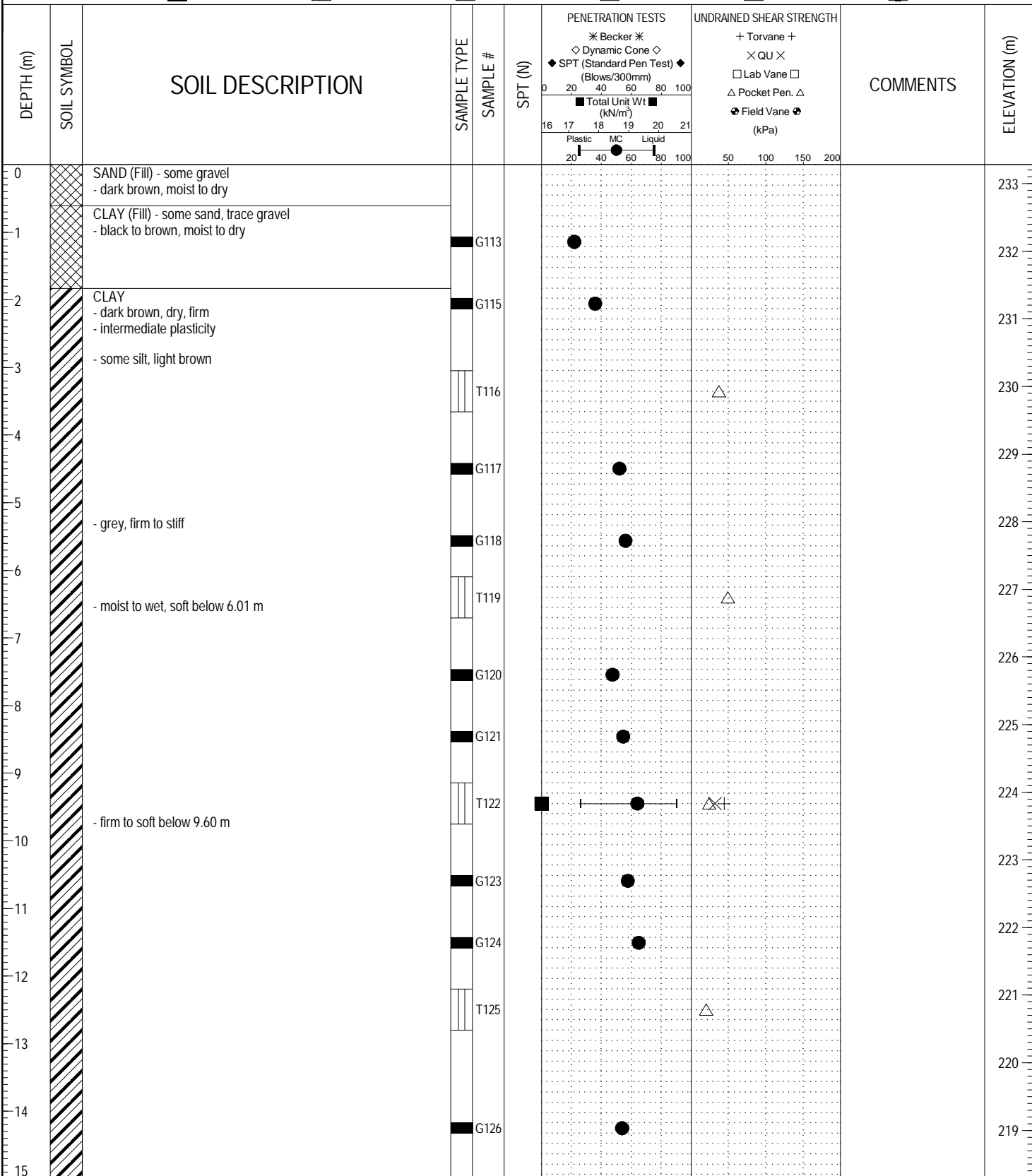
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 21.95 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/22
PROJECT ENGINEER: Zeyad Shukri	Page 2 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-D03
LOCATION: Plessis North Bound/CN Rail Intersection, East Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Mobile B-40, 125 mm SSA	ELEVATION (m): 233.28

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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LOGGED BY: Sam O.	COMPLETION DEPTH: 22.25 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/23
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-D03
LOCATION: Plessis North Bound/CN Rail Intersection, East Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Mobile B-40, 125 mm SSA	ELEVATION (m): 233.28

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input checked="" type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH	COMMENTS	ELEVATION (m)
						Becker	Dynamic Cone			
15										218
16										217
17										216
18		- some gravel, trace cobbles below 17.98 m		G127						215
19										214
20		LIMESTONE DOLOMITIC (Bedrock) - light grey to white, mottled yellow, core angle: 90 degrees - fine to medium grained, no foliation - close spacing, rough undulating joints, unaltered joints - R2 to R3 (weak to medium strong) - fossiliferous, vuggy - healed joint - slightly altered joint below 20.12 m		C1					- C1 ROD: 73% - Core Recovery: 92%	213
21										212
22		- rough planar joint		C2					- C2 ROD: 60% - Core Recovery: 94%	211
23		END OF TEST HOLE AT 21.95 m IN BEDROCK Notes: 1. Power auger refusal at 18.90 m below ground surface on BEDROCK. 2. HQ coring below 18.90 m. 3. Test hole backfilled with bentonite and auger cuttings.								210
24										209
25										208
26										207
27										206
28										205
29										204
30										204

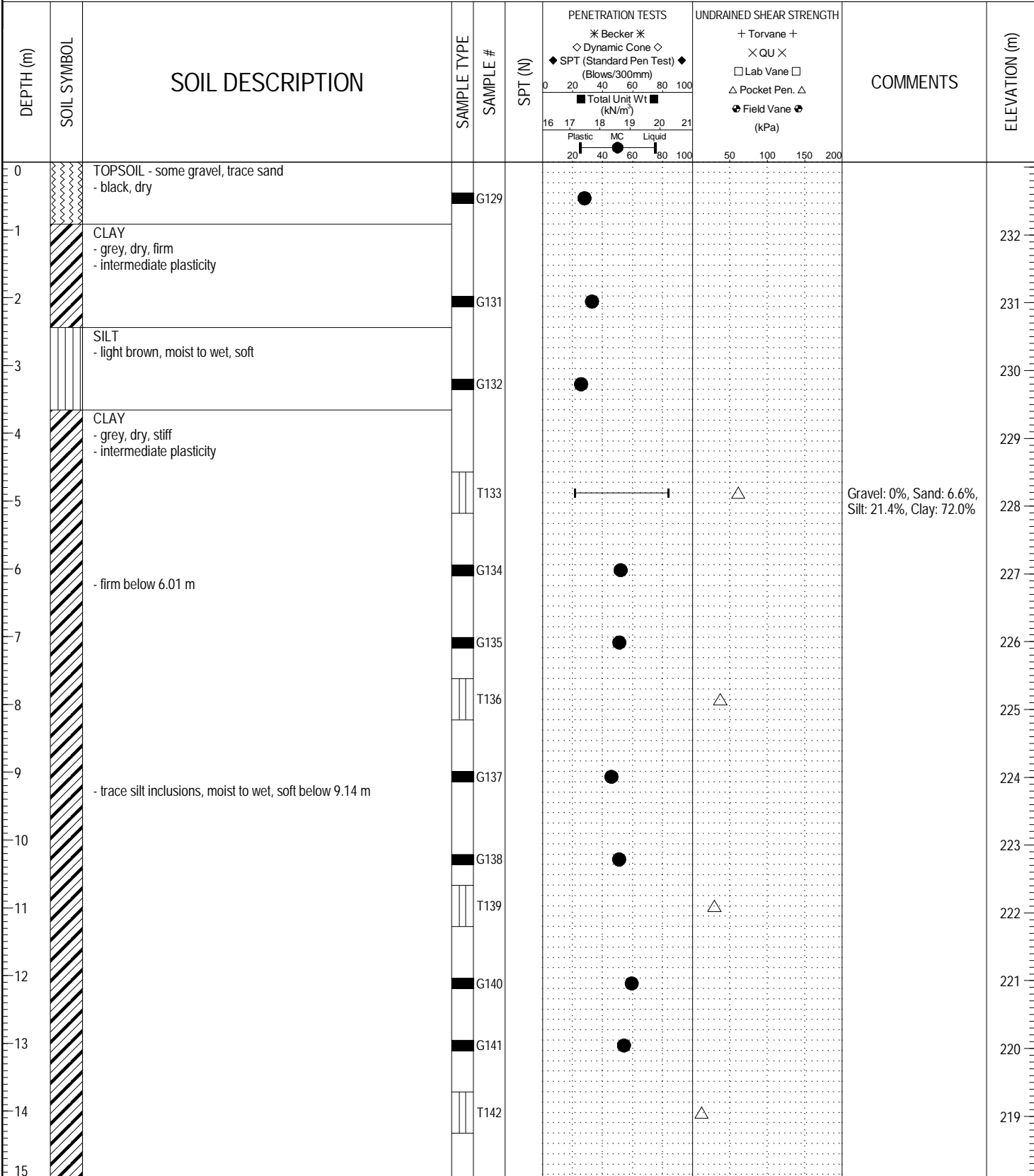
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 22.25 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/23
PROJECT ENGINEER: Zeyad Shukri	Page 2 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-D04
LOCATION: Plessis North Bound/CN Rail Intersection, East Shoulder Lawn		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Mobile B-40, 175 mm HSA	ELEVATION (m): 233.08

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 23.77 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/24
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-D04
LOCATION: Plessis North Bound/CN Rail Intersection, East Shoulder Lawn		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Mobile B-40, 175 mm HSA	ELEVATION (m): 233.08

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS	UNDRAINED SHEAR STRENGTH	COMMENTS	ELEVATION (m)
15									
16				G143					217
17		- trace gravel, wet below 16.76 m		G144					216
18		LIMESTONE (Bedrock) - light grey to white, core angle: 90 degrees - fine to medium grained, no foliation - moderately close spacing, rough undulating joints, unaltered joints		C1				- C1 RQD: 33% - Core Recovery: 82%	215
19		- R2 to R3 (weak to medium strong) - fossiliferous, filled vugs - high calcium limestone - rough planar joint		C2				- C2 RQD: 35% - Core Recovery: 100%	214
20				C3				- C3 RQD: 45% - Core Recovery: 100%	213
21				C4				- C4 RQD: 99% - Core Recovery: 100%	212
22									211
23									210
24		END OF TEST HOLE AT 23.77 m IN BEDROCK Notes: 1. Power auger refusal at 17.68 m below ground surface on BEDROCK. 2. HQ coring below 17.68 m. 3. Seepage observed at 16.76 m below ground surface. 4. Test hole backfilled with bentonite and auger cuttings.							209
25									208
26									207
27									206
28									205
29									204
30									

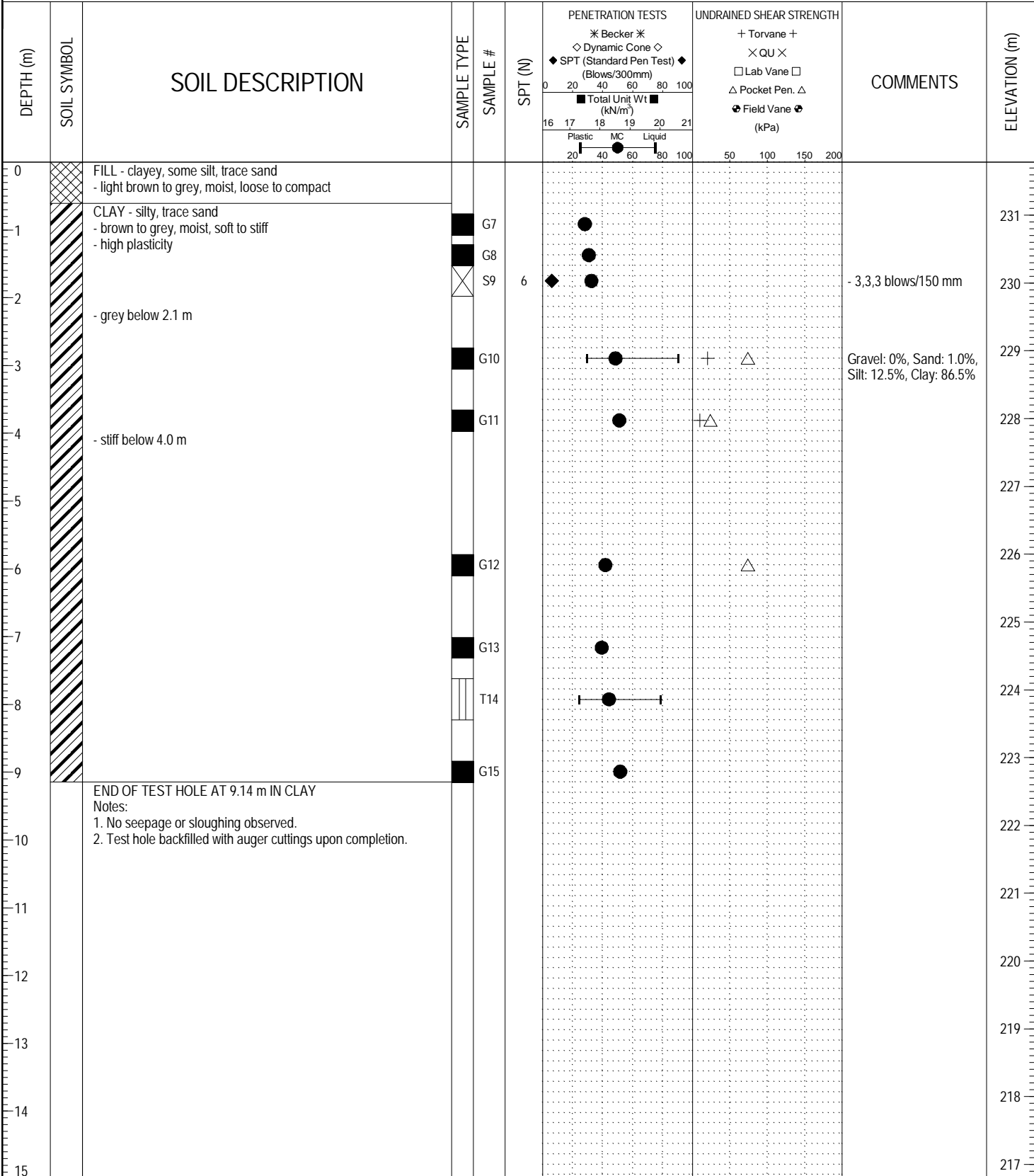
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 23.77 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/24
PROJECT ENGINEER: Zeyad Shukri	Page 2 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-I01
LOCATION: Plessis Road North Bound, East Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 231.78

SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
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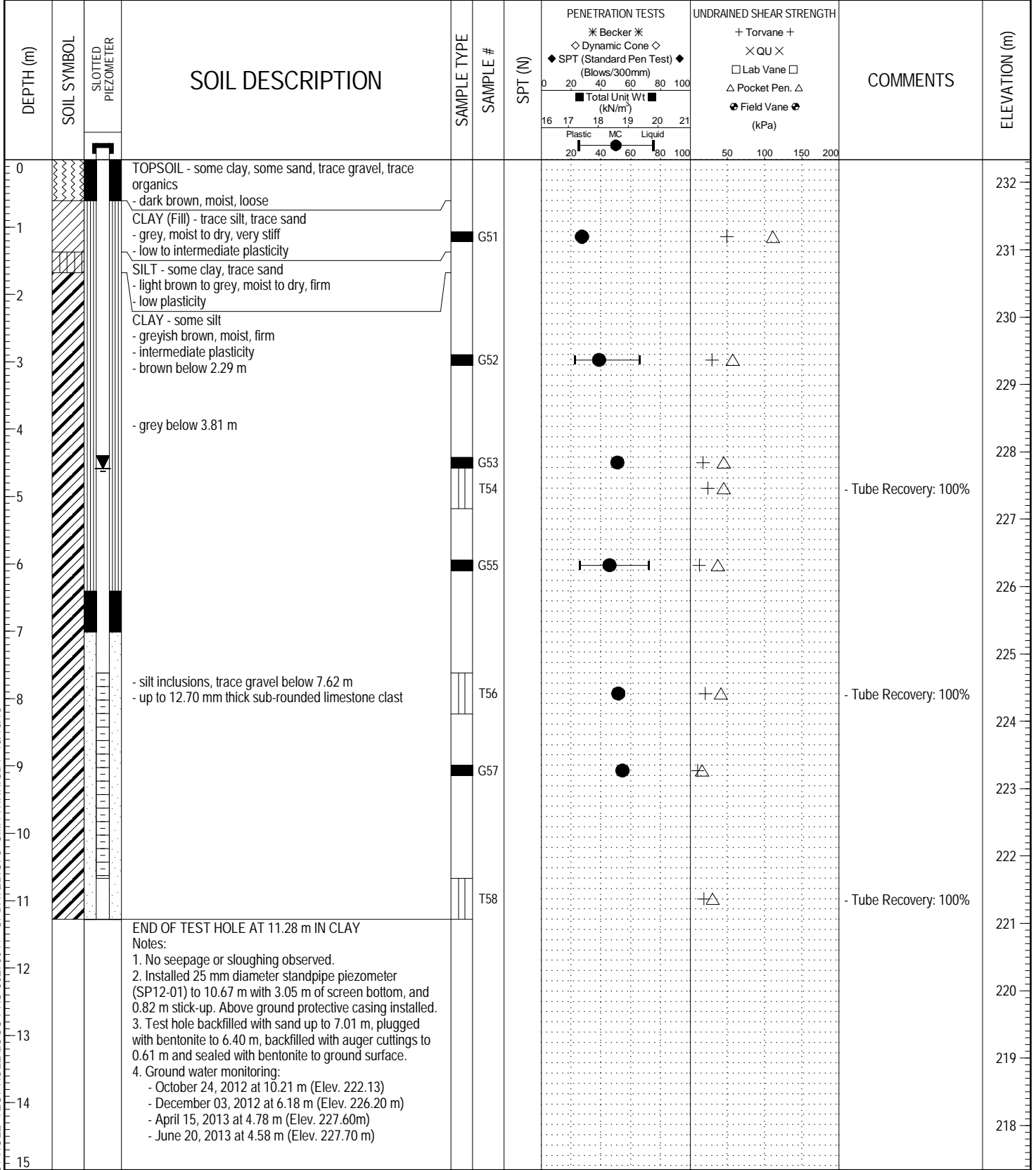


LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 9.14 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/9
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-I02
LOCATION: Plessis Road South Bound, West Shoulder Lawn		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.34
SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB <input type="checkbox"/> SHELBY TUBE <input type="checkbox"/> SPLIT SPOON <input type="checkbox"/> BULK <input type="checkbox"/> NO RECOVERY <input type="checkbox"/> CORE	
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE <input type="checkbox"/> GRAVEL <input type="checkbox"/> SLOUGH <input type="checkbox"/> GROUT <input type="checkbox"/> CUTTINGS <input type="checkbox"/> SAND	



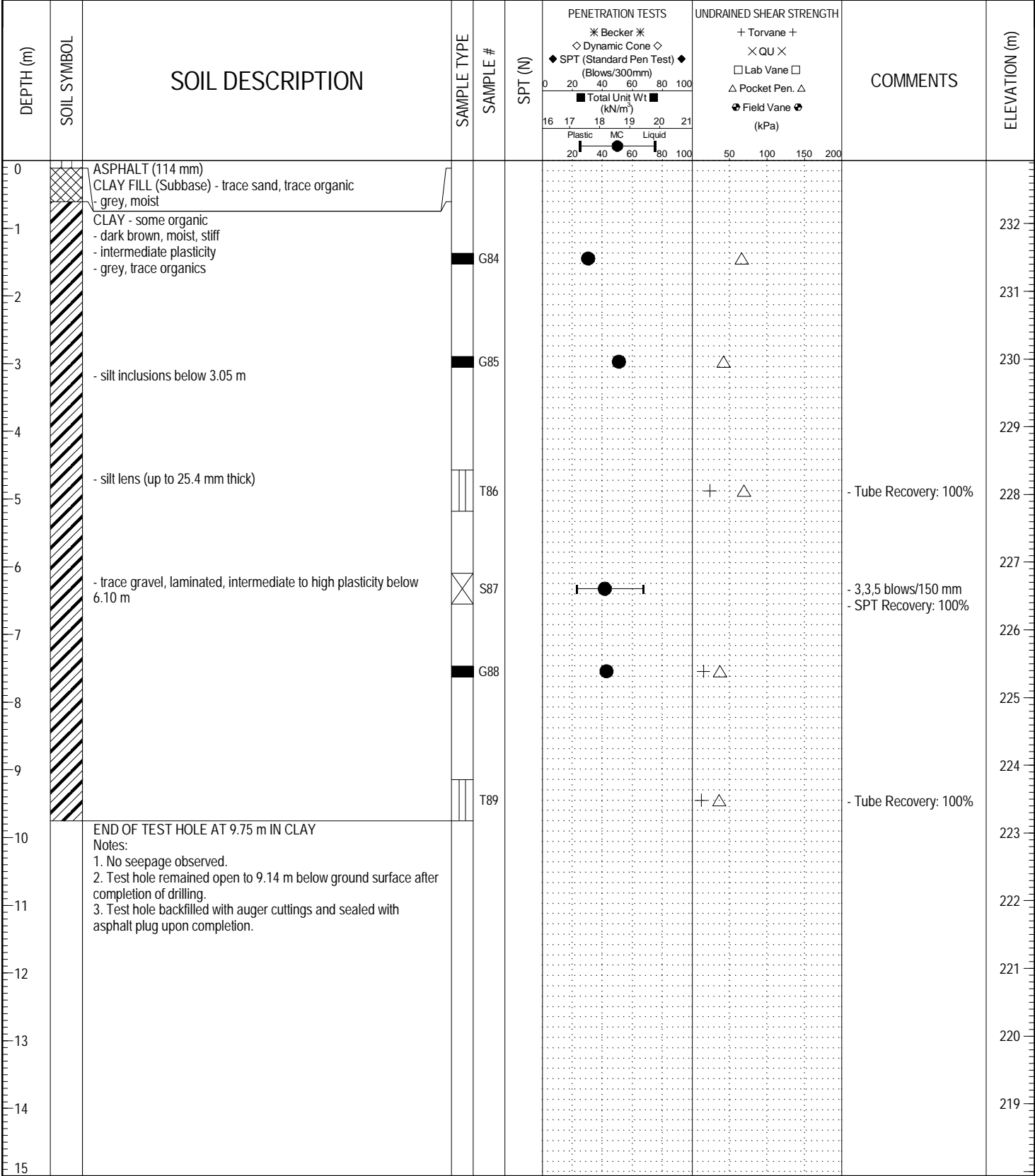
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 11.28 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/10
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-I03
LOCATION: Dugald Road East Bound, Curb Lane		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.93

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input checked="" type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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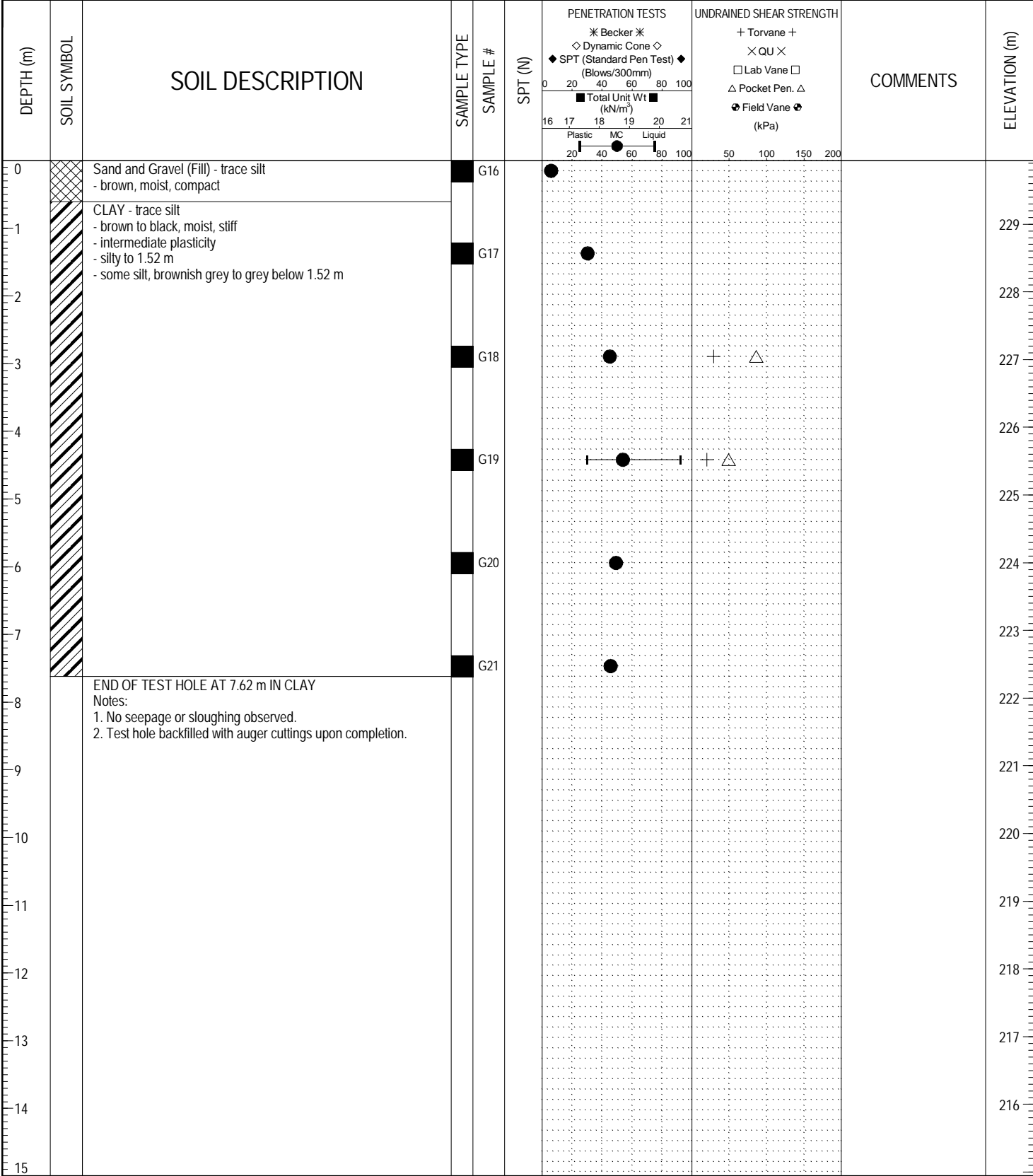
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 9.75 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/11/10
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-I05
LOCATION: Dugal Road East Bound, South Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 229.94

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE



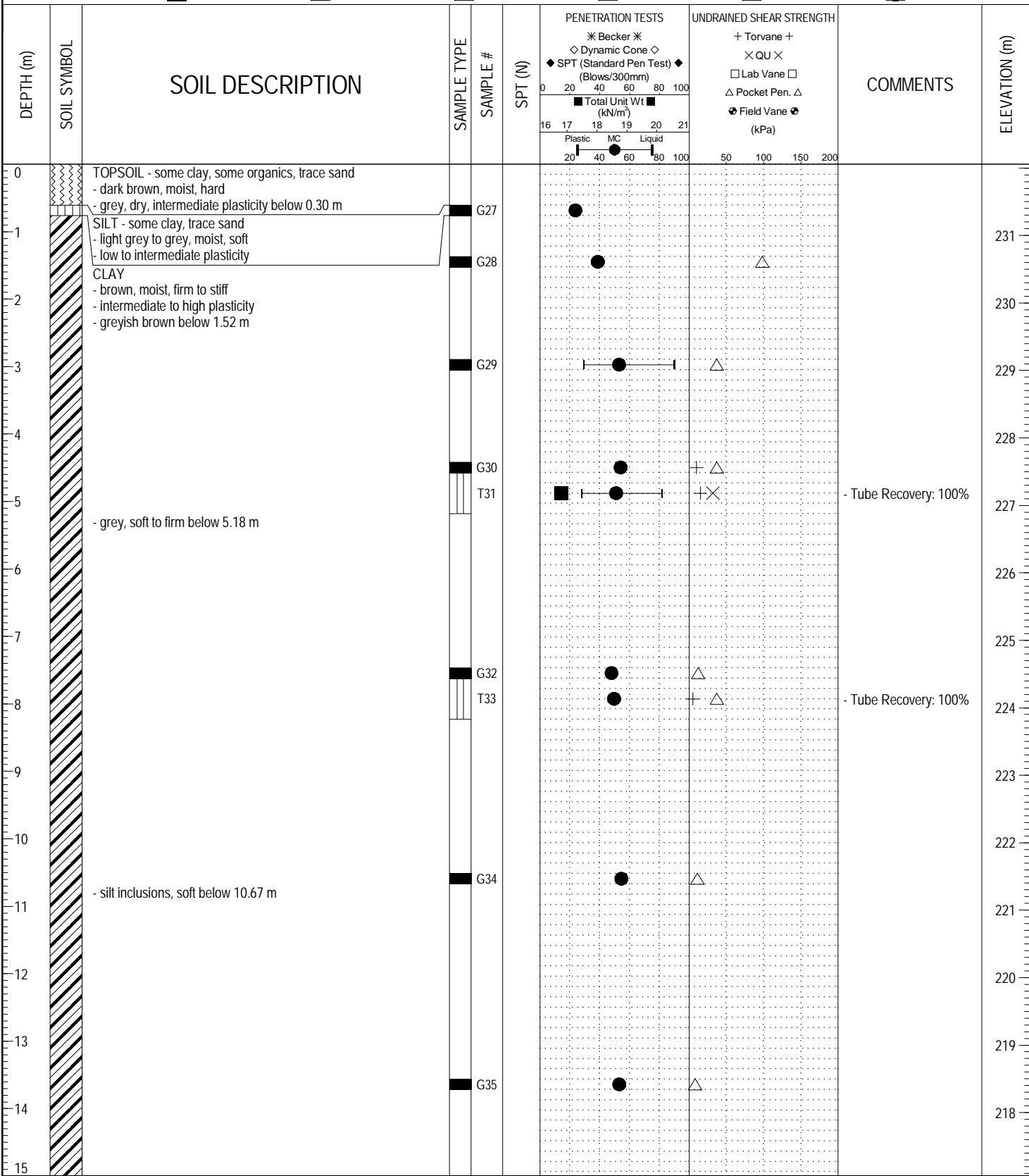
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 7.62 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/9
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-L01
LOCATION: East of Plessis Road		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.06

SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
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LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 17.98 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/10
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-L01
LOCATION: East of Plessis Road		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.06

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input checked="" type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS	UNDRAINED SHEAR STRENGTH	COMMENTS	ELEVATION (m)
15									216
16									215
17				G36					214
18		- limestone cobble up to 0.08 m thick		G37					213
18		END OF TEST HOLE AT 17.98 m ON BEDROCK							212
19		Notes: 1. Power auger refusal at 17.98 m below ground surface on BEDROCK. 2. Seepage observed at 10.97 m below ground surface. 3. Test hole remained open to 12.80 m below ground surface after completion of drilling. 4. Test hole backfilled with auger cuttings upon completion.							211
20									210
21									209
22									208
23									207
24									206
25									205
26									204
27									203
28									203
29									203
30									203

LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 17.98 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/10
PROJECT ENGINEER: Zeyad Shukri	Page 2 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S01
LOCATION: Plessis Road North Bound, Curb Lane		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.68

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input checked="" type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION (m)
						Becker * Dynamic Cone ◊ SPT (Standard Pen Test) ◆ (Blows/300mm)	Total Unit Wt (kN/m³)	Torvane + QU × Lab Vane □ Pocket Pen. △ Field Vane ⊕	(kPa)		
0		ASPHALT (114 mm) CONCRETE (Base) - grey, dry, bonded									232
1		SILT - clayey, trace sand - brown, moist, soft - low to intermediate plasticity		G165							231
2		CLAY - trace sand - brown, moist, stiff - intermediate plasticity, silt lenses (up to 25.4 mm thick dia.) - greyish brow, laminated below 1.52 m		G166							230
3				G167							229
4		- grey, firm below 3.05 m		S168	6	◆				- 2, 2, 4 blows/150 mm - SPT Recovery: 100%	228
5		- moist to wet below 3.96 m		G169							227
5		END OF TEST HOLE AT 4.57 m IN CLAY Notes: 1. No seepage or sloughing observed. 2. Test hole backfilled with auger cuttings and sealed with asphalt plug upon completion.									226
6											225
7											224
8											223
9											222
10											221
11											220
12											219
13											218
14											217
15											216

LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 4.57 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/31
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S02
LOCATION: Plessis Road South Bound, Curb Lane		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.39

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input checked="" type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION (m)
						Becker * Dynamic Cone ◊ SPT (Standard Pen Test) ◆ (Blows/300mm)	Total Unit Wt (kN/m³)	Torvane + QU × Lab Vane □ Pocket Pen. △ Field Vane ⊗	(kPa)		
0		ASPHALT (114 mm) CONCRETE (Base) - grey, dry, bonded									232
0.5		FILL (Subbase) - some clay, some sand, trace gravel - greyish black, moist, firm									
1		CLAY - brown, moist, stiff - intermediate plasticity, laminated		G170							231
2											230
3		- silt inclusions, firm below 3.05 m		G171							229
4		- silty sand pocket - greyish brown, trace gravel, trace oxidation below 3.66 m		G172							228
5				G173	6					- 2, 2, 4 blows/150 mm - SPT Recovery: 100%	228
5.03		END OF TEST HOLE AT 5.03 m IN CLAY		S174							227
6		Notes: 1. No seepage or sloughing observed. 2. Test hole backfilled with auger cuttings and sealed with asphalt plug upon completion.									227
7											226
8											225
9											224
10											223
11											222
12											221
13											220
14											219
15											218

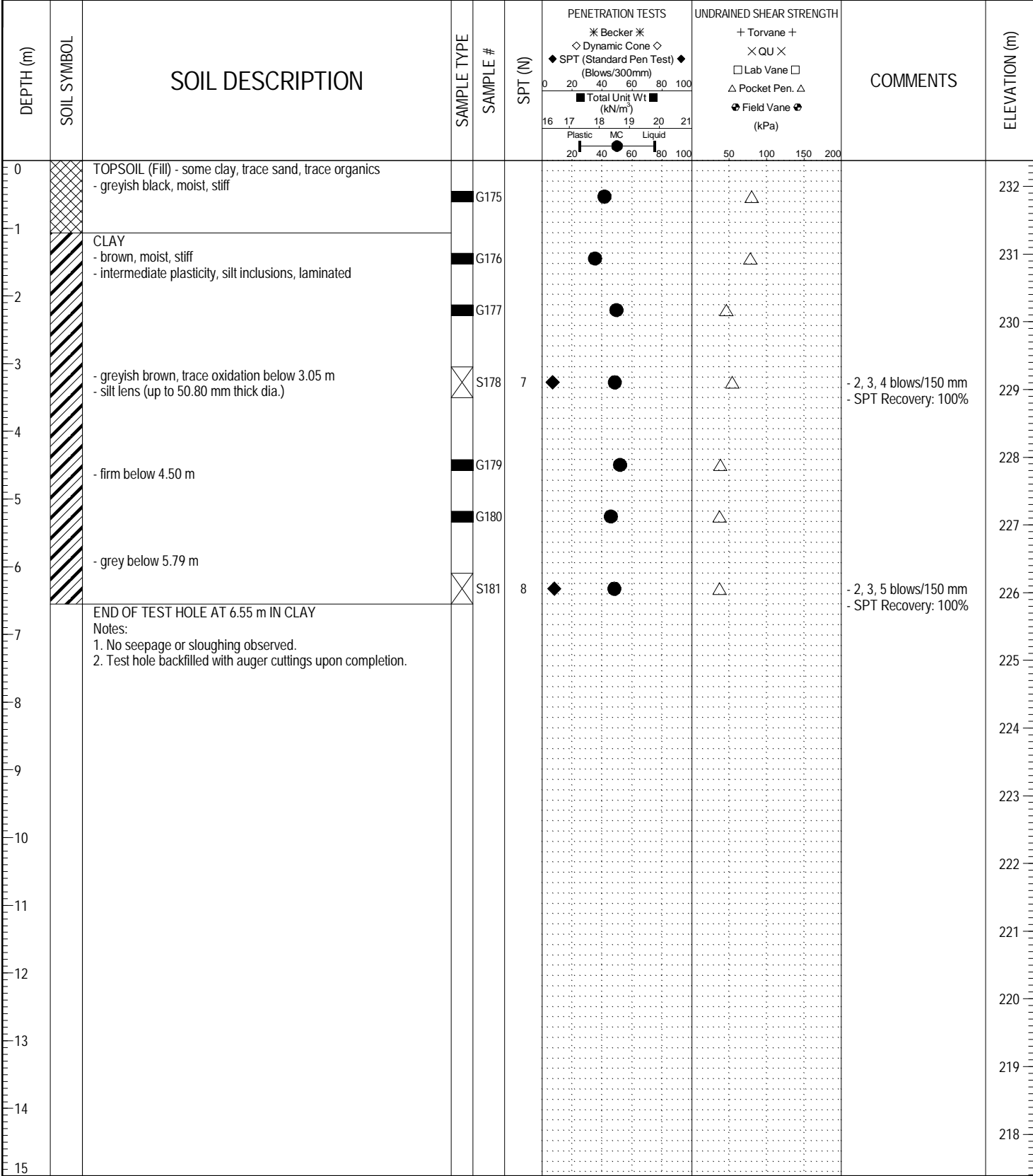
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 5.03 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/31
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S03
LOCATION: Plessis Road North Bound, East Shoulder Lawn		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.38

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE



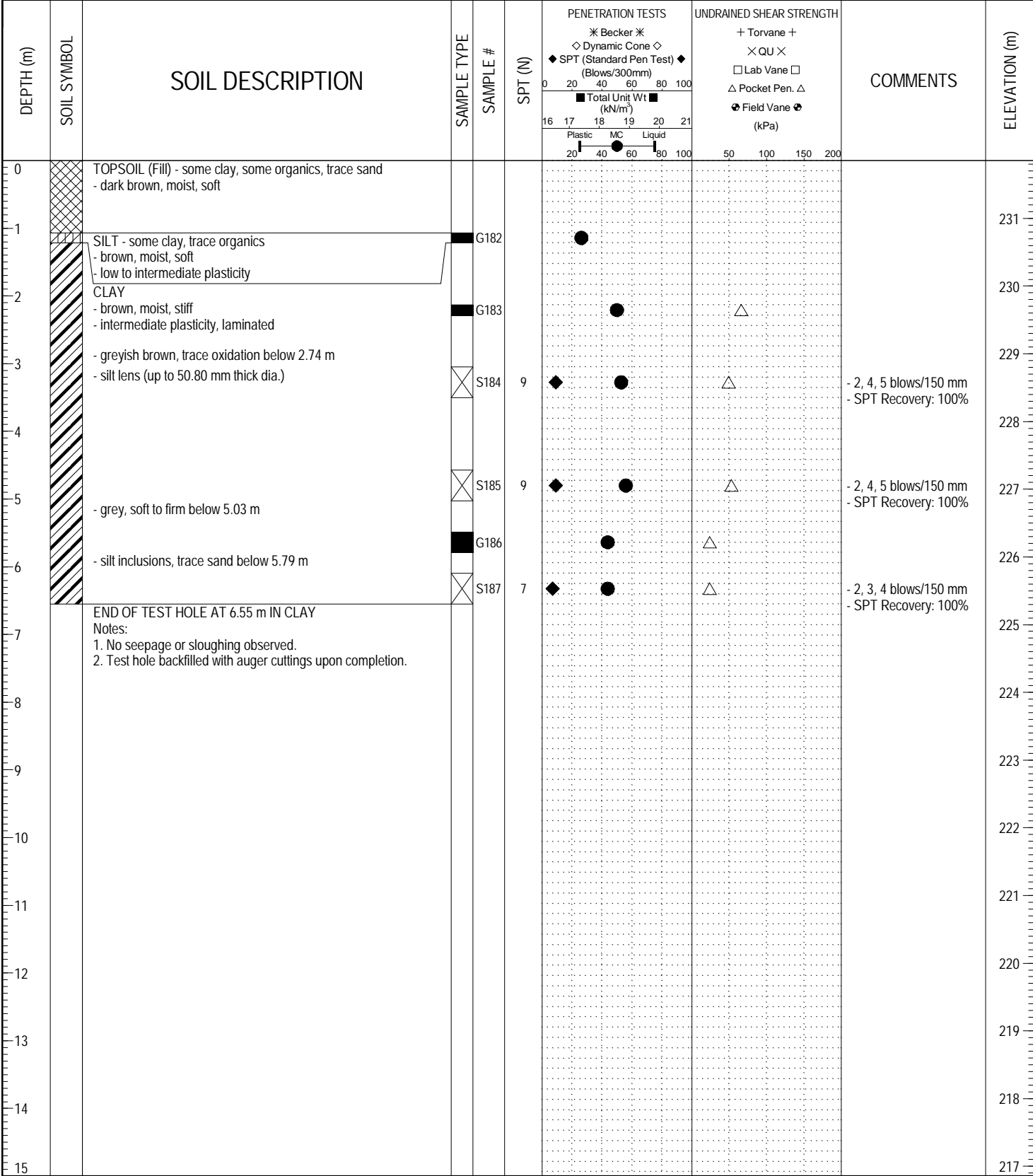
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 6.55 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/31
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S04
LOCATION: Plessis Road South Bound, West Shoulder Lawn		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 231.85

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE



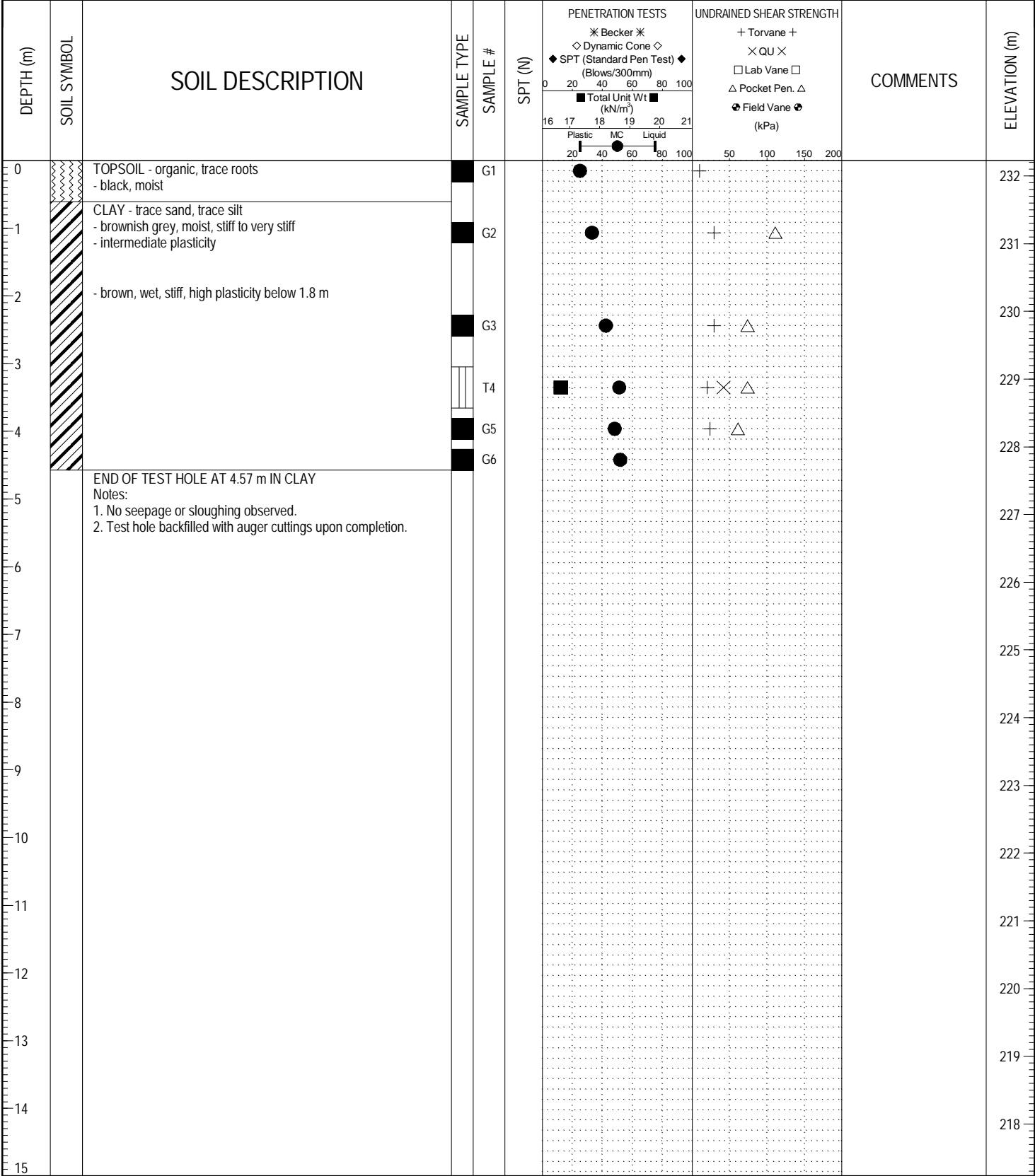
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 6.55 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/31
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S05
LOCATION: Plessis Road North Bound, East Shoulder Lawn		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.23

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE



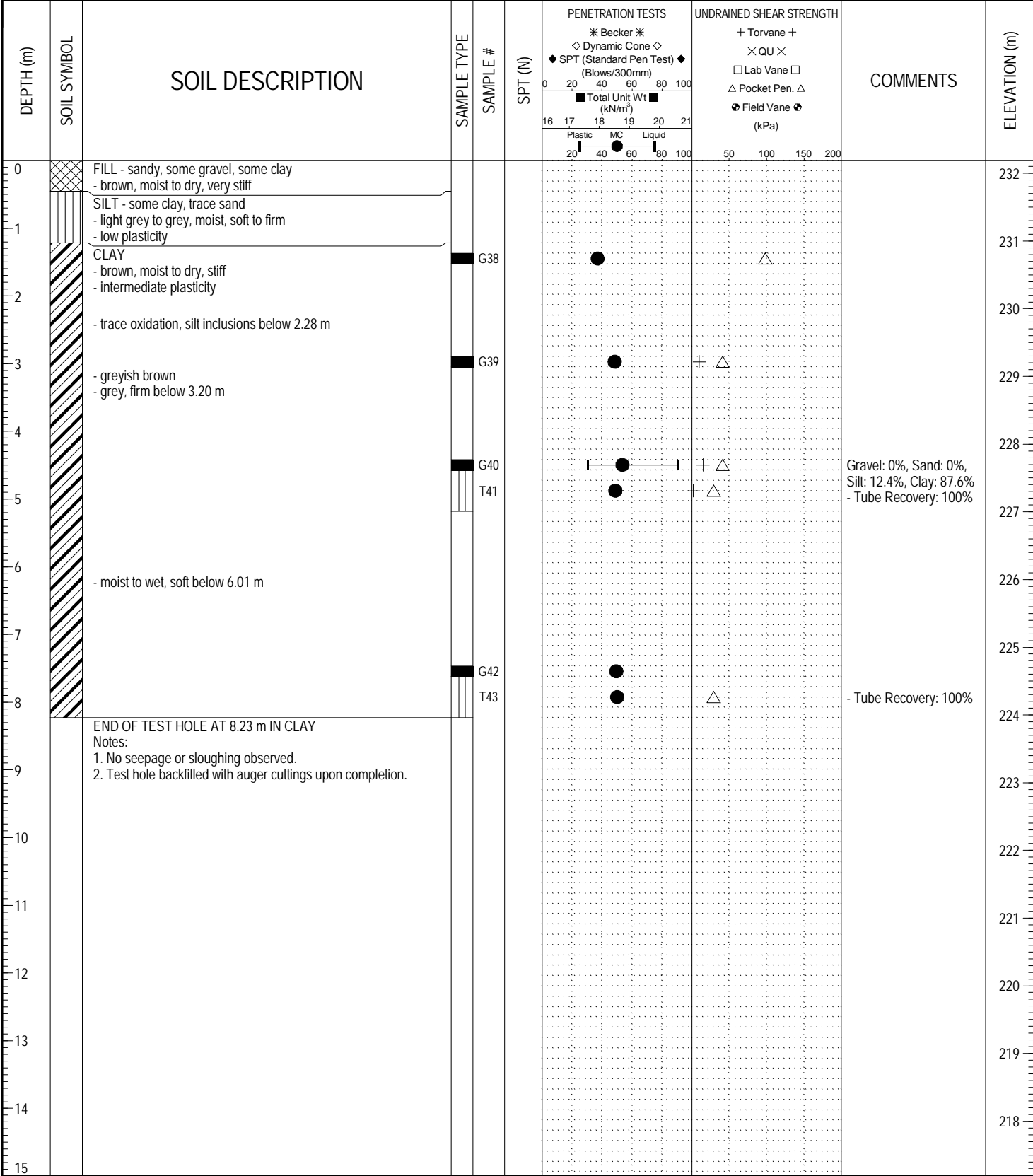
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 4.57 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/9
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass CLIENT: City of Winnipeg TESTHOLE NO: TH12-S07
 LOCATION: Plessis Road South Bound, West Shoulder Lawn PROJECT NO.: 60273041
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Track Mounted MP5, 125 mm SSA ELEVATION (m): 232.19

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE



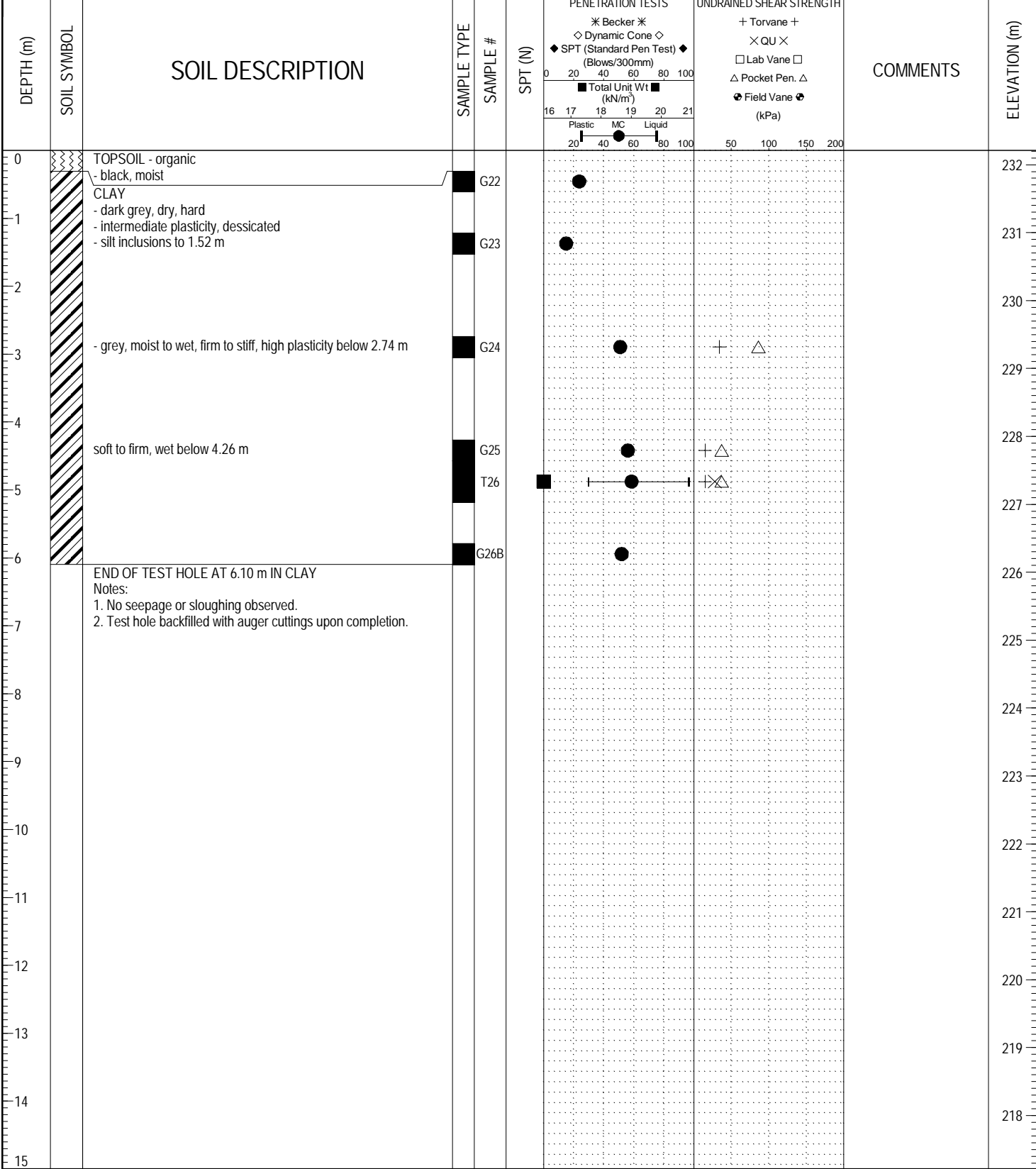
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O. COMPLETION DEPTH: 8.23 m
 REVIEWED BY: Omer Eissa COMPLETION DATE: 12/10/10
 PROJECT ENGINEER: Zeyad Shukri Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S08
LOCATION: Plessis Road North Bound, East Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.21

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE



END OF TEST HOLE AT 6.10 m IN CLAY
Notes:
1. No seepage or sloughing observed.
2. Test hole backfilled with auger cuttings upon completion.

LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 6.10 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/9/10
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S09
LOCATION: Plessis/Dugald Intersection, North East Corner Lawn		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Mobile B-40, 125 mm SSA	ELEVATION (m): 232.26

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS	UNDRAINED SHEAR STRENGTH	COMMENTS	ELEVATION (m)
0		TOPSOIL - some clay, some organics, trace sand - dark brown, moist							232
1		CLAY - trace sand - brown, moist, stiff - intermediate plasticity - silt lens (25.4 mm thick) - greyish brown, silt inclusions, firm, trace oxidation below 1.52 m		G158		●	△		231
2									230
3		- grey, intermediate to high plasticity below 3.35 m		G159		●	△	- 1, 2, 3 blows/150 mm - SPT Recovery: 100%	229
4				S160		●	△		228
5				G161		●	△		227
6				S162		●	△		226
7								225	
8				G163		●	△	224	
9								223	
10		END OF TEST HOLE AT 9.60 m IN CLAY Notes: 1. No seepage or sloughing observed. 2. Test hole backfilled with auger cuttings and sealed with bentonite at ground surface upon completion.		S164		●	△	- 1, 2, 3 blows/150 mm - SPT Recovery: 100%	222
11									221
12									220
13									219
14									218
15									218

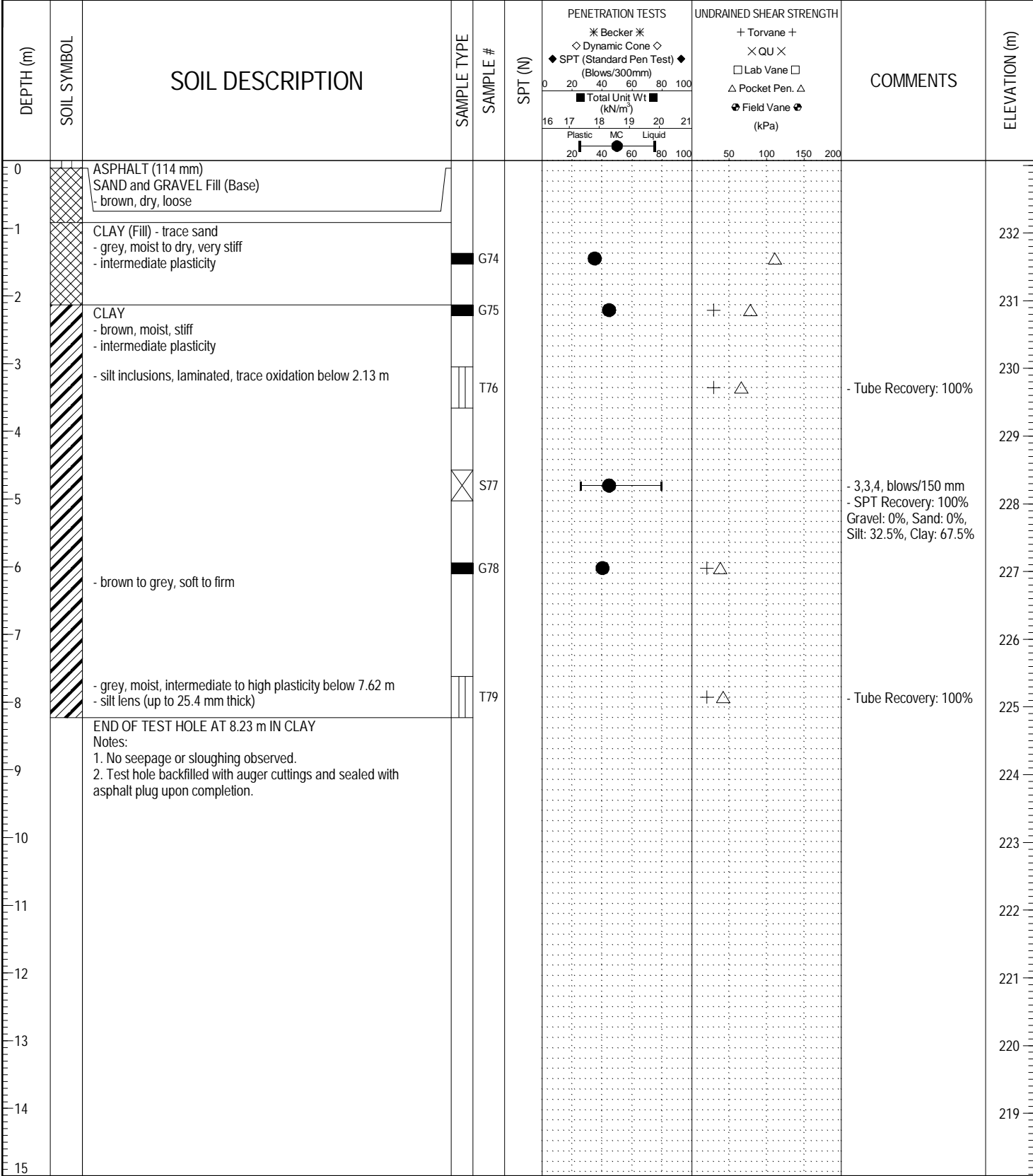
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 9.60 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/27
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S10
LOCATION: Dugald Road West Bound, Curb Lane		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 233.07

SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
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LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 8.23 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/11
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S11
LOCATION: Dugald Road West Bound, North Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.65

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS	UNDRAINED SHEAR STRENGTH	COMMENTS	ELEVATION (m)
0		SAND and GRAVEL (Fill) - trace clay, trace organics - brown, dry, loose							232
1		CLAY - trace sand, trace gravel - grey, moist, stiff - intermediate plasticity - silt inclusions, silt lens (up to 51 mm thick) below 1.52 m		G80					231
3				S81	7			- 2,3,4 blows/150 mm - SPT Recovery: 100%	229
5		- greyish brown, trace oxidation, laminated below 4.27 m		T82				- Tube Recovery: 100%	228
6		END OF TEST HOLE AT 6.10 m IN CLAY		G83					227
7		Notes: 1. No seepage observed. 2. Test hole remained open to 4.57 m below ground surface after completion of drilling. 3. Test hole backfilled with auger cuttings upon completion.							226
8									225
9									224
10									223
11									222
12									221
13									220
14									219
15									218

LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 6.10 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/11/10
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S12
LOCATION: Dugald Road West Bound, North Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.99

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input checked="" type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION (m)
						Becker	Dynamic Cone	Torvane	QU		
0		SAND and GRAVEL (Fill) - trace clay, trace organics - brown, moist, loose									
1		CLAY (Fill) - trace gravel, trace sand - grey, moist to dry, stiff to very stiff - intermediate plasticity									232
2				G71							231
3		- brown, very stiff, intermediate to high plasticity - silt seam (0.61 m thick) - grey, wet, oxidized - low plasticity		G72							230
3.35				T73							229
4		END OF TEST HOLE AT 3.35 m IN CLAY Notes: 1. Seepage observed at 0.30 m below ground surface. 2. No sloughing observed. 3. Test hole backfilled with auger cuttings and sealed with bentonite upon completion.									228
5											227
6											226
7											225
8											224
9											223
10											222
11											221
12											220
13											219
14											
15											

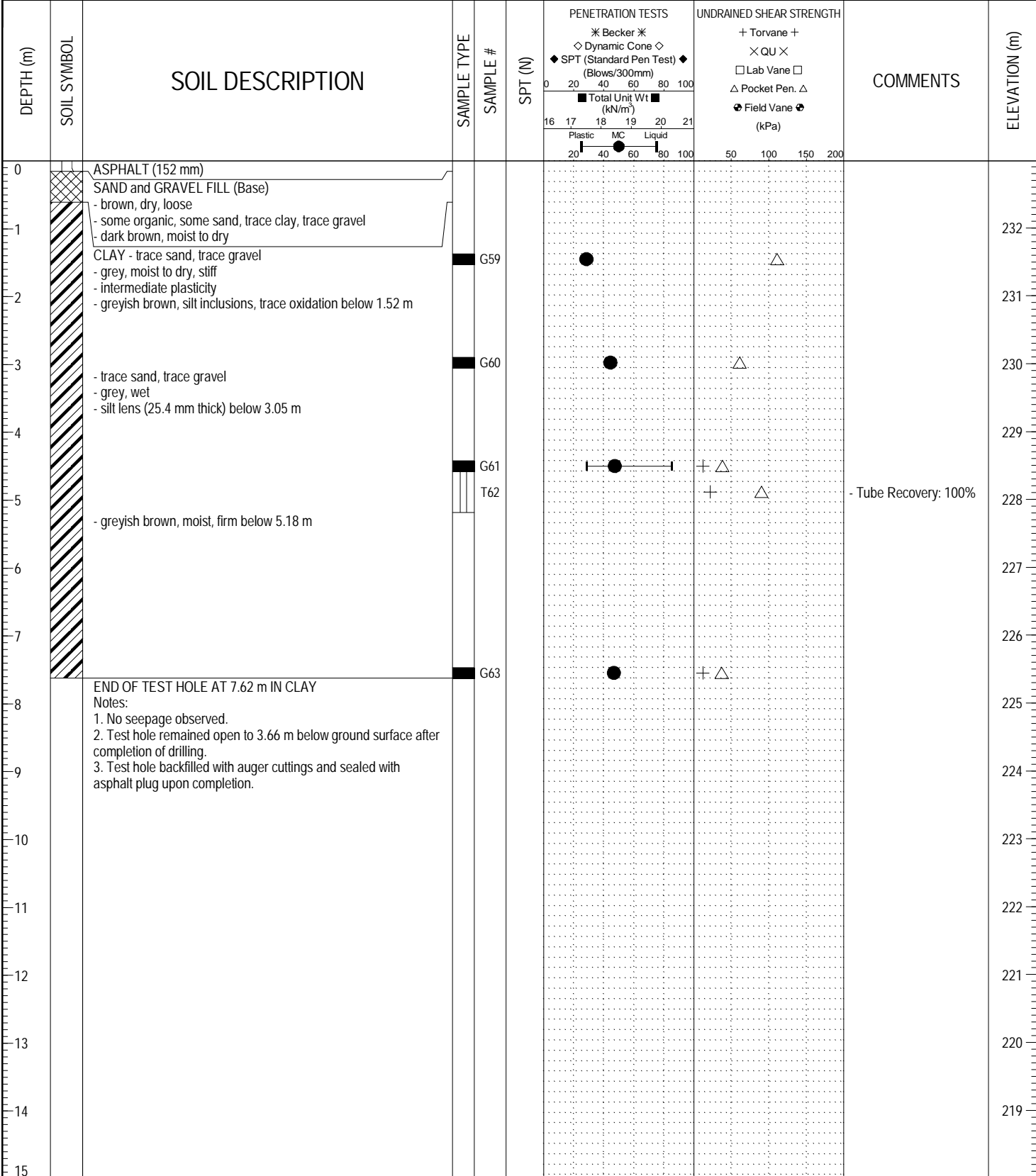
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 3.35 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/11
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S13
LOCATION: Dugald Road East Bound, Curb Lane		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.99

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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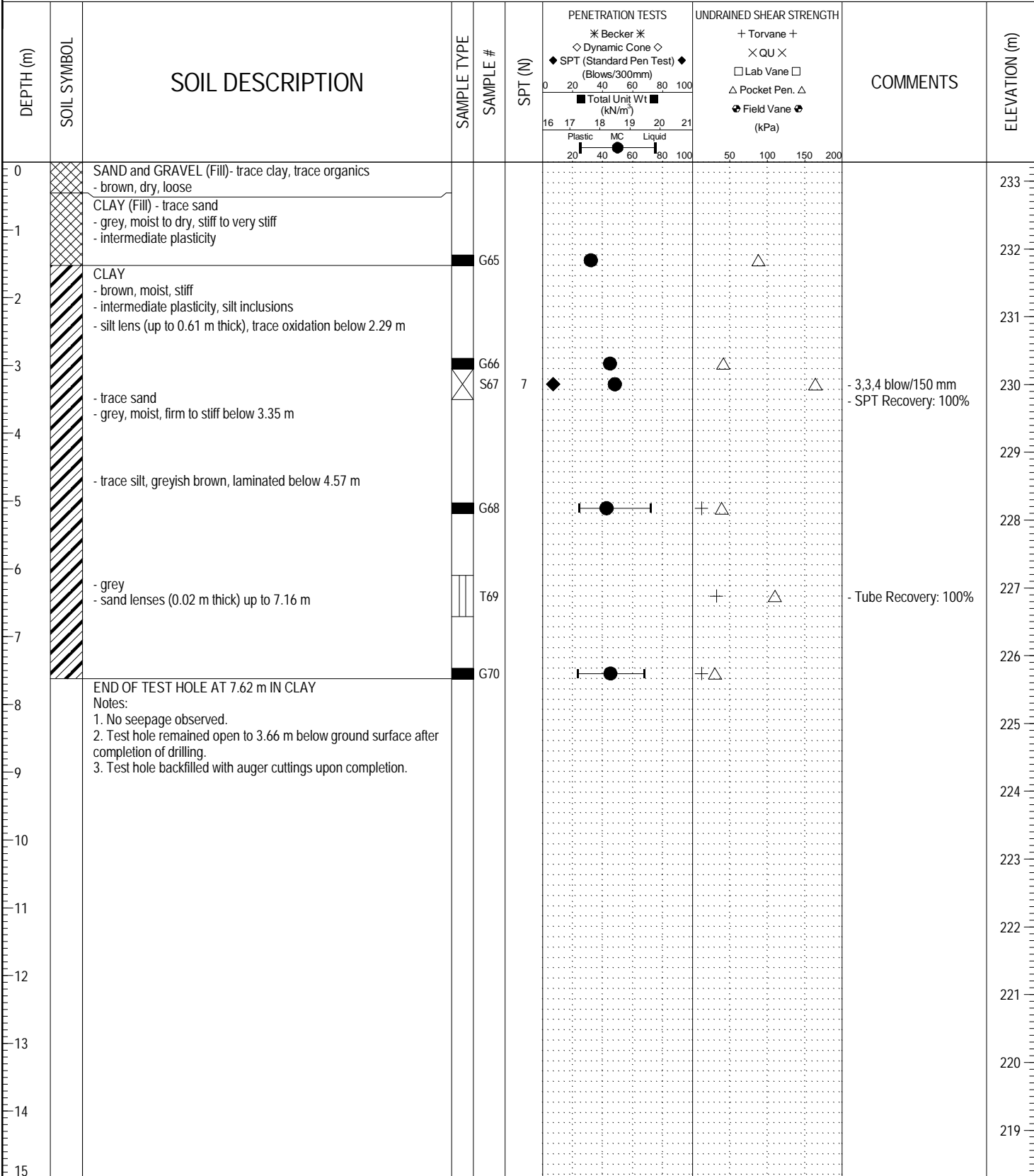
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 7.62 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/11
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S14
LOCATION: Dugald Road West Bound, North Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 233.28

SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
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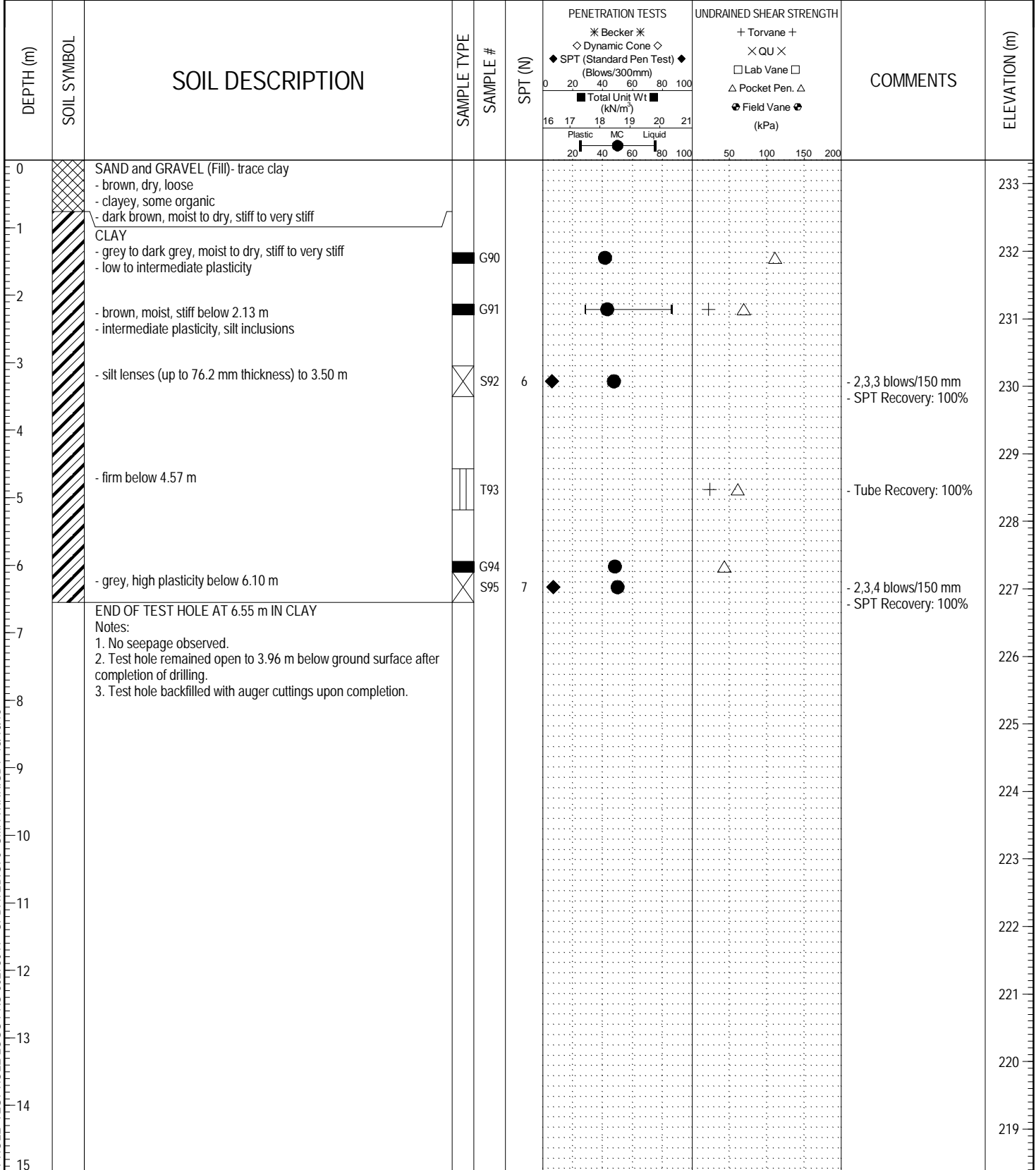
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 7.62 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/11
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S15
LOCATION: Plessis Road South Bound, West Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 233.35

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input checked="" type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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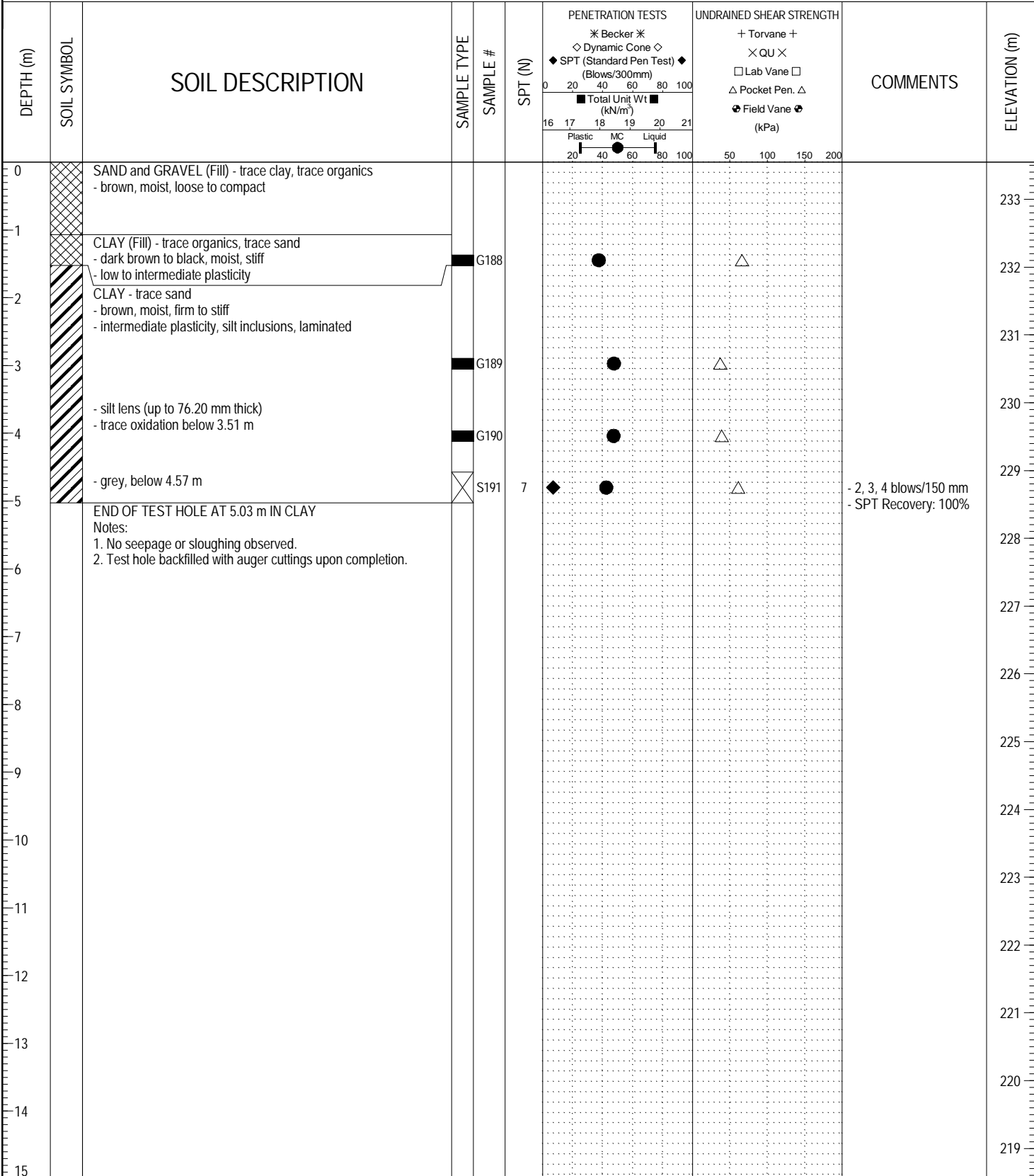
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 6.55 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/11
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S16
LOCATION: Plessis Road South Bound, West Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 233.55

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input checked="" type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 5.03 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/31
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S17
LOCATION: Plessis Road South Bound, West Shoulder		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 233.53

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION (m)
						Becker * Dynamic Cone ◊ SPT (Standard Pen Test) ◆ (Blows/300mm)	Total Unit Wt (kN/m ³)	Torvane + QU × Lab Vane □ Pocket Pen. △ Field Vane ⊗	(kPa)		
0		SAND and GRAVEL (Fill) - trace clay, trace organics - brown, moist, loose to compact									233
1		CLAY (Fill) - trace organics, trace sand - dark brown to black, moist, stiff - low to intermediate plasticity	<input checked="" type="checkbox"/>	G192							232
2		CLAY - brown, moist, stiff - intermediate plasticity, silt inclusions, laminated	<input checked="" type="checkbox"/>	G193							231
3		- greyish brown, firm below 3.05 m - sand and silt lens (up to 63.50 mm thick)	<input checked="" type="checkbox"/>	S194	4					- 1, 1, 3 blows/150 mm - SPT Recovery: 100%	230
4		- trace gravel below 3.96 m	<input checked="" type="checkbox"/>	G195							229
5		END OF TEST HOLE AT 4.57 m IN CLAY Notes: 1. No seepage or sloughing observed. 2. Test hole backfilled with auger cuttings upon completion.									228
6											227
7											226
8											225
9											224
10											223
11											222
12											221
13											220
14											219

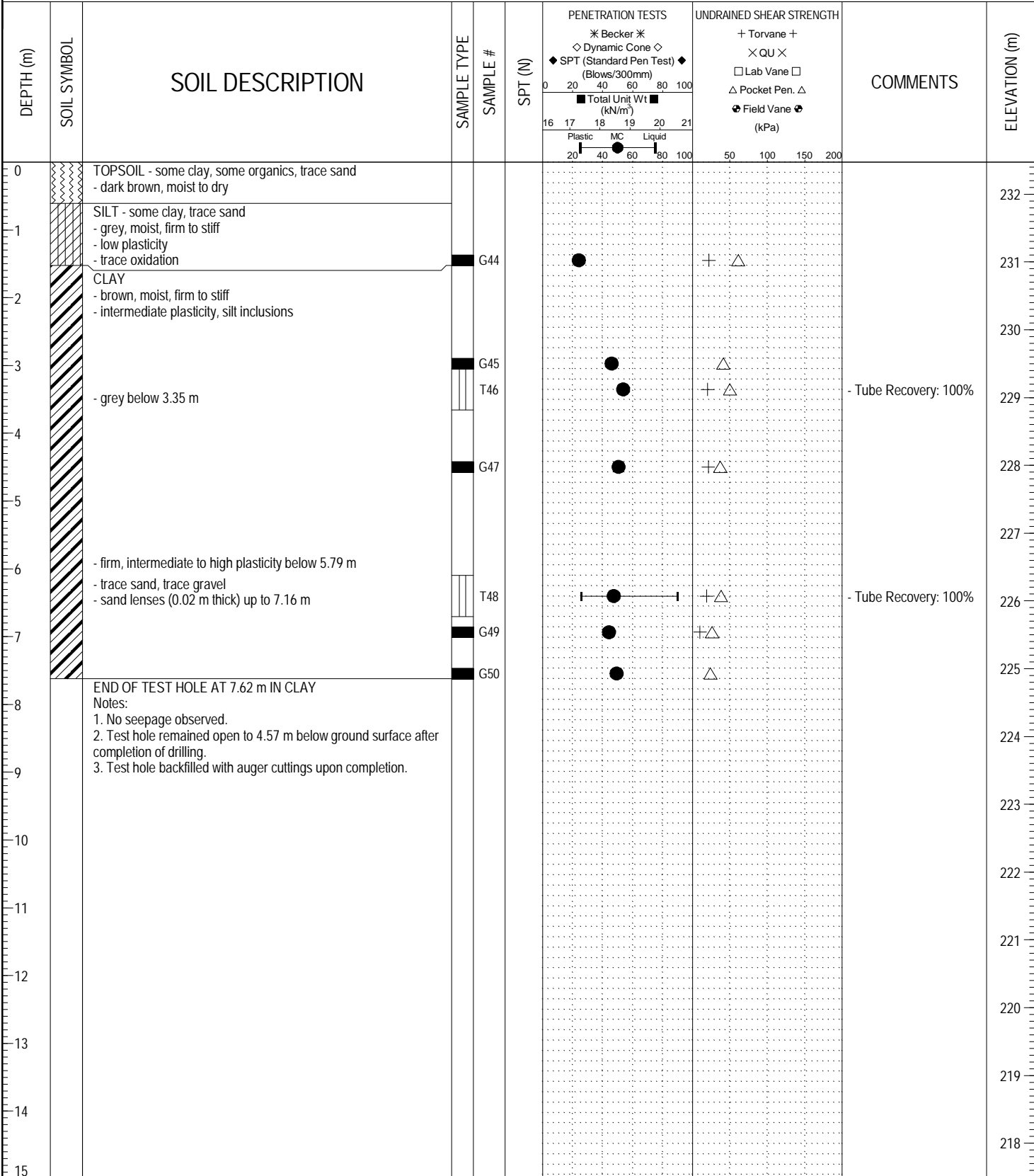
LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 4.57 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/31
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH12-S18
LOCATION: Plessis/Dugald Intersection, South West Corner Lawn		PROJECT NO.: 60273041
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Track Mounted MP5, 125 mm SSA	ELEVATION (m): 232.47

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> SHELBY TUBE	<input checked="" type="checkbox"/> SPLIT SPOON	<input type="checkbox"/> BULK	<input checked="" type="checkbox"/> NO RECOVERY	<input type="checkbox"/> CORE
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LOG OF TEST HOLE TEST HOLE LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/16



LOGGED BY: Sam O.	COMPLETION DEPTH: 7.62 m
REVIEWED BY: Omer Eissa	COMPLETION DATE: 12/10/10
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 1

P:\160273041\1000-CADD\102-SHEETS\B\160273041-FIG-00-0000-B-TestholeLocPlan.dwg



AECOM



**PLESSIS
UNDERPASS STUDY**

Supplemental Testhole Location Plan

0 37.5 75 150m
SCALE: 1:5000

B-002

PROJECT: Plessis Road Underpass CLIENT: City of Winnipeg TESTHOLE NO: TH13-B01
 LOCATION: Plessis East Abutment, N: 5528000.9 E: 641834.1 PROJECT NO.: 60273041
 CONTRACTOR: Paddock Drilling Ltd. METHOD: Track Mounted Acker SS 3, 125 mm SSA ELEVATION (m): 233.54

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH (kPa)	COMMENTS	ELEVATION
						Becker	Dynamic Cone			
0		SAND and GRAVEL (Fill) - some silt, some clay - brown, moist, compact								233
1				G14						232
2		CLAY - trace gravel - brown, moist, firm - high plasticity		G15						231
3		SILT - trace gravel - grey, moist, soft - low to intermediate plasticity								230
4		CLAY - trace gravel - brown, moist, firm - high plasticity - greyish brown, silt inclusions below 4.6 m		G16						229
5				G17						228
6				G18						227
7		- grey, soft below 7.0 m		G19						226
8				G20						225
9				G21						224
10				G22						223
11				G23						222
12				G24						221
13										220
14										219
15										218
16										217
17		- gravelly below 16.8 m								216
18										216

LOG OF TEST HOLE SUPPLEMENTAL INVESTIGATION-BRIDGE TEST HOLE LOGS-PRU-60273041.GPJ UMA WINN.GDT 8/7/13



LOGGED BY: Sam Oshati COMPLETION DEPTH: 24.69 m
 REVIEWED BY: Zeyad Shukri COMPLETION DATE: 7/30/13
 PROJECT ENGINEER: Zeyad Shukri Page 1 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH13-B01
LOCATION: Plessis East Abutment, N: 5528000.9 E: 641834.1		PROJECT NO.: 60273041
CONTRACTOR: Paddock Drilling Ltd.	METHOD: Track Mounted Acker SS 3, 125 mm SSA	ELEVATION (m): 233.54
SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB <input type="checkbox"/> SHELBY TUBE <input checked="" type="checkbox"/> SPLIT SPOON <input type="checkbox"/> BULK <input type="checkbox"/> NO RECOVERY <input type="checkbox"/> CORE	

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) 0 20 40 60 80 100 ■ Total Unit Wt ■ (kN/m ³) 16 17 18 19 20 21 Plastic MC Liquid 20 40 60 80 100	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ● (kPa) 50 100 150 200				
18		LIMESTONE (Bedrock)		G25						C1 RQD: 22% Core Recovery: 64%	215
19		- light grey to white, core angle: 90 degrees		C2						C2 RQD: 51% Core Recovery: 88%	214
20		- fine to medium grained, no foliation		C3						C3 RQD: 79% Core Recovery: 92%	213
21		- close to moderately close spacing, rough undulating joints, unaltered joints		C4						C4 RQD: 79% Core Recovery: 94%	212
22		- R2 to R3 (weak to medium strong)		C5						C5 RQD: 93% Core Recovery: 98%	211
23		- fossiliferous									210
24		- fractured to 20.1 m (Elev. 213.4) below ground surface									209
25		- competent rock (RQD > 70%) below 20.1 m									208
25		END OF TEST HOLE AT 24.69 m IN BEDROCK									207
26		Notes:									206
27		1. Power auger refusal at 18.05 m below ground surface on BEDROCK.									205
28		2. HQ coring below 18.05 m.									204
29		3. Test hole sealed with bentonite up to 3.05 m and grouted from 3.05 to ground surface.									203
30											202
31											201
32											200
33											199
34											198

LOG OF TEST HOLE SUPPLEMENTAL INVESTIGATION-BRIDGE TEST HOLE LOGS-PRU-60273041.GPJ UMA WINN.GDT 8/7/13



LOGGED BY: Sam Oshati	COMPLETION DEPTH: 24.69 m
REVIEWED BY: Zeyad Shukri	COMPLETION DATE: 7/30/13
PROJECT ENGINEER: Zeyad Shukri	Page 2 of 2

PROJECT: Plessis Road Underpass CLIENT: City of Winnipeg TESTHOLE NO: **TH13-B02**
 LOCATION: Plessis North Pier, N: 5527999.0 E: 641663.6 PROJECT NO.: 60273041
 CONTRACTOR: Paddock Drilling Ltd. METHOD: Track Mounted Acker SS 3, 125 mm SSA ELEVATION (m): 232.96

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH	COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt ■ (kN/m ³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ⊕ Field Vane ⊕ (kPa)			
0		ASPHALT (300 mm)								
0-1		SAND and GRAVEL (Base) - light brown, dry, compact - medium to coarse grained								232
1-2		CLAY (Fill) - some gravel, some sand, trace organics - brown, moist, firm - Intermediate plasticity		G1				+		231
2-3				G2						230
3-4		ORGANICS - wood chips - brown to black, moist to wet - hydrocarbon (diesel fuel)		G3						229
4-5				G4						228
5-6		CLAY - greyish brown, moist, firm - high plasticity		G5						227
6-7				G6						226
7-8		- grey, trace silt inclusions, soft below 7.62 m		G7						225
8-9				G8						224
9-10				G9						223
10-11		- trace gravel below 11 m		G10						222
11-12				G11						221
12-13				G12						220
13-14				G13						219
14-15										218
15-16										217
16-17										216
17-18		- silty, wet, some gravel								

LOG OF TEST HOLE SUPPLEMENTAL INVESTIGATION-BRIDGE TEST HOLE LOGS-PRU-60273041.GPJ UMA WINN.GDT 8/7/13



LOGGED BY: Sam Oshati COMPLETION DEPTH: 26.21 m
 REVIEWED BY: Zeyad Shukri COMPLETION DATE: 7/31/13
 PROJECT ENGINEER: Zeyad Shukri Page 1 of 2

PROJECT: Plessis Road Underpass CLIENT: City of Winnipeg TESTHOLE NO: TH13-B02
 LOCATION: Plessis North Pier, N: 5527999.0 E: 641663.6 PROJECT NO.: 60273041
 CONTRACTOR: Paddock Drilling Ltd. METHOD: Track Mounted Acker SS 3, 125 mm SSA ELEVATION (m): 232.96

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

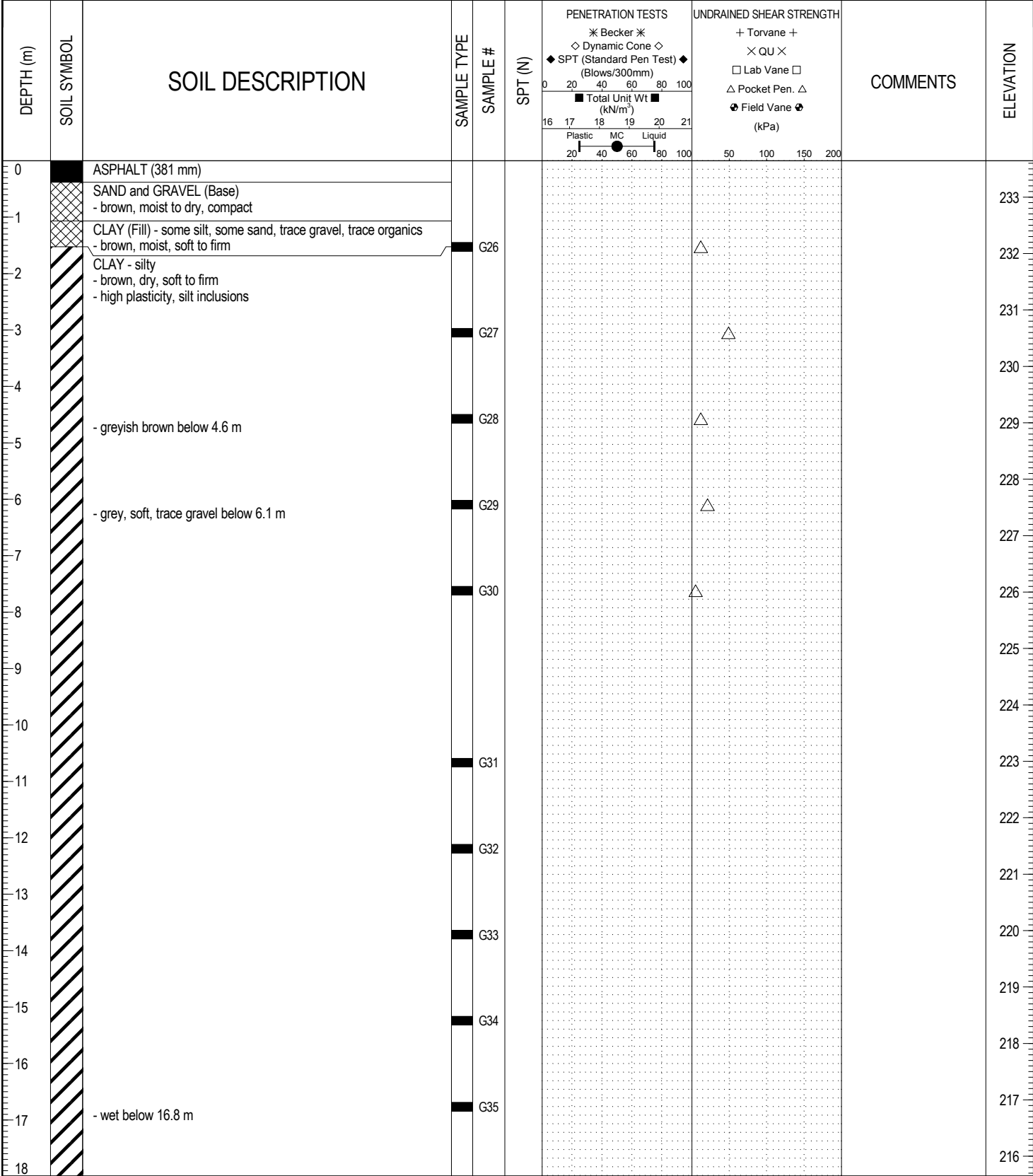
DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH	COMMENTS	ELEVATION
						UNDRAINED SHEAR STRENGTH				
18		- cobbly, some boulders below 17.7 m								
19		LIMESTONE (Bedrock) - light grey, core angle: 90 degrees - fine to medium grained, no foliation - close to moderately close spacing, rough undulating joints, unaltered joints		C1					C1 RQD: 40% Core Recovery: 70%	214
20		- R2 to R3 (weak to medium strong) - fossiliferous, vuggy to 21.6 m - fractured to 21.6 m (Elev. 211.4) below ground surface		C2					C2 RQD: 48% Core Recovery: 93%	213
21				C3					C3 RQD: 75% Core Recovery: 92%	212
22		- competent rock (RQD > 70%) below 21.6 m - mottled yellow to 21.95 m		C4					C4 RQD: 81% Core Recovery: 90%	211
23				C5					C5 RQD: 85% Core Recovery: 96%	210
24										209
25										208
26										207
27		END OF TEST HOLE AT 26.21 m IN BEDROCK Notes: 1. Power auger refusal at 18.5 m below ground surface on BEDROCK. 2. HQ coring below 18.5 m. 3. Seepage observed at 17.5 m below ground surface. 4. Test hole grouted up to 18.3 m and sealed with bentonite to ground surface.								206
28										205
29										204
30										203
31										202
32										201
33										200
34										199
35										198
36										

LOG OF TEST HOLE SUPPLEMENTAL INVESTIGATION-BRIDGE TEST HOLE LOGS-PRU-60273041.GPJ UJMA WINN.GDT 8/7/13



LOGGED BY: Sam Oshati COMPLETION DEPTH: 26.21 m
 REVIEWED BY: Zeyad Shukri COMPLETION DATE: 7/31/13
 PROJECT ENGINEER: Zeyad Shukri Page 2 of 2

PROJECT: Plessis Road Underpass		CLIENT: City of Winnipeg		TESTHOLE NO: TH13-B03	
LOCATION: Plessis South Pier, N: 5527960.9 E: 641831.2				PROJECT NO.: 60273041	
CONTRACTOR: Paddock Drilling Ltd.			METHOD: Track Mounted Acker SS 3, 125 mm SSA		ELEVATION (m): 233.64
SAMPLE TYPE		GRAB	SHELBY TUBE	SPLIT SPOON	BULK
		NO RECOVERY	CORE		



LOGGED BY: Sam Oshati	COMPLETION DEPTH: 24.69 m
REVIEWED BY: Zeyad Shukri	COMPLETION DATE: 8/1/13
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 2

PROJECT: Plessis Road Underpass CLIENT: City of Winnipeg TESTHOLE NO: **TH13-B03**
 LOCATION: Plessis South Pier, N: 5527960.9 E: 641831.2 PROJECT NO.: 60273041
 CONTRACTOR: Paddock Drilling Ltd. METHOD: Track Mounted Acker SS 3, 125 mm SSA ELEVATION (m): 233.64

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH	COMMENTS	ELEVATION	
						Becker	Dynamic Cone				Lab Vane
18				G36						215	
19				G37						214	
20		LIMESTONE (Bedrock) - light grey to white, core angle: 90 degrees - fine to medium grained, no foliation - close to moderately close spacing, rough undulating joints, unaltered joints - R2 to R3 (weak to medium strong) - fossiliferous, vuggy - fractured to 21.6 m (Elev. 212.0) below ground surface - competent rock (RQD > 70%) below 21.6 m		C1					C1 RQD: 15% Core Recovery: 45%	213	
21				C2						C2 RQD: 62% Core Recovery: 97%	212
22					C3						211
23					C4						210
24										209	
25		END OF TEST HOLE AT 24.69 m IN BEDROCK Notes: 1. Power auger refusal at 19.2 m below ground surface on BEDROCK. 2. HQ coring below 19.2 m. 3. Seepage observed at 16.8 m below ground surface. 4. Test hole sealed with bentonite up to 19.8 m and grouted from 19.8 m to ground surface.								208	
26										207	
27										206	
28										205	
29										204	
30										203	
31										202	
32										201	
33										200	
34										199	
35										198	
36										198	

LOG OF TEST HOLE SUPPLEMENTAL INVESTIGATION-BRIDGE TEST HOLE LOGS-PRU-60273041.GPJ UJMA WINN.GDT 8/7/13



LOGGED BY: Sam Oshati COMPLETION DEPTH: 24.69 m
 REVIEWED BY: Zeyad Shukri COMPLETION DATE: 8/1/13
 PROJECT ENGINEER: Zeyad Shukri Page 2 of 2

PROJECT: Plessis Road Underpass		CLIENT: City of Winnipeg		TESTHOLE NO: TH13-B04	
LOCATION: Plessis West Abutment, N: 5527982.0 E: 641811.9				PROJECT NO.: 60273041	
CONTRACTOR: Paddock Drilling Ltd.			METHOD: Track Mounted Acker SS 3, 125 mm SSA		ELEVATION (m): 233.00
SAMPLE TYPE		GRAB	SHELBY TUBE	SPLIT SPOON	BULK
		NO RECOVERY	CORE		

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Becker	Dynamic Cone	Torvane	QU		
0		SAND and GRAVEL (Fill) - trace organics - brown, dry to moist, compact									
1		CLAY (Fill) - some sand, some gravel, trace organics - dark brown to brown, moist, firm - intermediate plasticity		G38							232
2		SILT - light brown, moist, soft - low to intermediate plasticity CLAY - brown, moist, firm - high plasticity - silty to 3.4 m		G39							231
3				G40							230
4		- greyish brown below 4.6 m		G41							229
5		- grey below 5.2 m		G42							228
6				G43							227
7				G44							226
8				G45							225
9		- silt inclusions, moist to wet below 9.1 m		G46							224
10				G47							223
11		- moist below 10.7 m		G48							222
12				G49							221
13				G50							220
14		- moist to wet below 13.7 m									219
15											218
16											217
17											216
18											

LOG OF TEST HOLE SUPPLEMENTAL INVESTIGATION-BRIDGE TEST HOLE LOGS-PRU-60273041.GPJ UJMA WINN.GDT 8/7/13



LOGGED BY: Sam Oshati	COMPLETION DEPTH: 30.78 m
REVIEWED BY: Zeyad Shukri	COMPLETION DATE: 8/2/13
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 2

PROJECT: Plessis Road Underpass	CLIENT: City of Winnipeg	TESTHOLE NO: TH13-B04
LOCATION: Plessis West Abutment, N: 5527982.0 E: 641811.9		PROJECT NO.: 60273041
CONTRACTOR: Paddock Drilling Ltd.	METHOD: Track Mounted Acker SS 3, 125 mm SSA	ELEVATION (m): 233.00
SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB <input type="checkbox"/> SHELBY TUBE <input checked="" type="checkbox"/> SPLIT SPOON <input type="checkbox"/> BULK <input type="checkbox"/> NO RECOVERY <input type="checkbox"/> CORE	

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) 0 20 40 60 80 100 ■ Total Unit Wt ■ (kN/m ³) 16 17 18 19 20 21 Plastic MC Liquid 20 40 60 80 100	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ● (kPa) 50 100 150 200				
18											
19		LIMESTONE (Bedrock)		G51							214
20		- light grey to white, core angle: 90 degrees - fine to medium grained, no foliation - close to moderately close spacing, rough undulating joints, unaltered joints		C1						C1 RQD: 56% Core Recovery: 75%	213
21		- R2 to R3 (weak to medium strong) - fossiliferous - fractured to 20.1 m (Elev. 212.9) below ground surface - competent rock below 20.1 m - mottled yellow to 21.8 m		C2						C2 RQD: 82% Core Recovery: 96%	212
22				C3						C3 RQD: 92% Core Recovery: 98%	211
23				C4						C4 RQD: 78% Core Recovery: 95%	210
24				C5						C5 RQD: 64% Core Recovery: 75%	209
25				C6						C6 RQD: 80% Core Recovery: 98%	208
26		- ripple marks to 26.4 m		C7						C7 RQD: 81% Core Recovery: 99%	207
27				C8						C8 RQD: 94% Core Recovery: 99%	206
28											205
29											204
30											203
31		END OF TEST HOLE AT 30.78 m IN BEDROCK									202
32		Notes:									201
33		1. Power auger refusal at 18.9 m below ground surface on BEDROCK.									200
34		2. HQ coring below 18.9 m.									199
35		3. Seepage observed at 15.24 m below ground surface.									198
36		4. sloughing observed at 19.8 m below ground surface in rock.									
		5. Test hole grouted up to 19.8 m and sealed with bentonite from 19.8 m to ground surface.									

LOG OF TEST HOLE SUPPLEMENTAL INVESTIGATION-BRIDGE TEST HOLE LOGS-PRU-60273041.GPJ UJMA WINN.GDT 8/7/13



LOGGED BY: Sam Oshati	COMPLETION DEPTH: 30.78 m
REVIEWED BY: Zeyad Shukri	COMPLETION DATE: 8/2/13
PROJECT ENGINEER: Zeyad Shukri	Page 2 of 2

Memorandum

To	Eric Loewen, P.Eng	Page	1
CC			
Subject	Summary of Test Caisson Investigation - Plessis Road Underpass Project		
From	Zeyad Shukri		
Date	September 5, 2013	Project Number	60273041 (404.19.1.1)

A test caisson was advanced to verify the design assumptions, examine the feasibility of construction and assist in the selection of adequate equipment and proper construction practices. The drilling took place during the period between July 5th and July 9th, 2013. The test caisson was advanced on the west shoulder of Plessis Road south of the existing CN railway right-of-way as shown in Figure 1, Appendix A. Drilling was carried out by Subterranean (Manitoba) Ltd. using a track-mounted Soilmec SR-65 piling rig equipped with a 940 mm diameter flight auger and 760 mm core barrel. Due to the size and heavy weight of the drill rig, a pad was constructed using granular rock fill to support the weight of the equipment. The test caisson was advanced through the overburden with augers to practical refusal near the bedrock surface at a depth of 17.8 m below surface or approximate elevation 214.7 m. The core barrel was then employed to core into the bedrock to a termination depth of 78.5 feet (23.9 m) below ground surface or approximate elevation of 208.6 m.

The caisson was sleeved with an outer safety casing 4 feet (1.2 m) in diameter. The outer safety casing extended from ground surface to a depth of 25 feet (7.6 m) below surface. An inner sleeve was inserted into the test caisson to protect the walls of the test hole at deeper depths. The inner sleeve was 36 inch (0.91 m) in diameter and extended into the weathered zone of the bedrock to a depth of 69 feet (21 m) below surface. The rock socket below depth 69 feet (21 m) was advanced without the use of a sleeve or casing to support the side walls of the caisson.

The soil stratigraphy at the test caisson location consisted of a thin layer of topsoil underlain by a thick lacustrine clay deposit extending to approximately 17.8 m below ground surface. The clay was firm to soft in consistency and of high plasticity. Limestone bedrock was encountered at 17.8 m below ground surface. No noticeable till layer was observed between the clay deposit and the limestone bedrock. The top 3.8 m of the bedrock was weathered (poor quality) and consisted of highly permeable rubble and fractured rock. Competent bedrock (fair quality) was encountered at a depth of 21.6 m below ground surface or approximate elevation of 210.9 m. A detailed log showing the soil strata encountered is provided in Appendix A. Photos taken during the drilling are attached in Appendix B.

Very significant water inflow in the test caisson was observed from the weathered bedrock zone. The water in the test caisson stabilized at 10.6 m below the ground surface upon completion of drilling (i.e. elevation of 221.9 m). The test caisson was backfilled with 30 MPa concrete from termination depth up to 11.5 m below ground surface. Stabilized fill was used to backfill the hole from the depth of 11.5 m up to ground surface.

Caisson advancement was completed in approximately 12 hours of drilling. Additional time was required for site preparation including a granular pad placement at the caisson location, carrying out a pumping test post drilling and backfilling the caisson with concrete and stabilized fill.

For production caissons, the uncased socket length should be a minimum of one socket diameter within sound, competent bedrock. The minimum shaft diameter of the rock socket should not be less than 760 mm and the maximum diameter should be selected to suit the locally available coring equipment. The rock sockets should not be spaced closer than 2.5 socket diameters, centre to centre.

To summarize, based on observations from the test caisson drilling, the following practices are recommended for the installation of the bridge caissons:

- Sleeving from ground surface to the bedrock contact as a minimum, and sufficiently into the significantly weathered bedrock as required to maintain a stable excavation.
- Due to difficulties noted when retrieving the rock cores from the bottom of the caisson, a special core barrel was necessary to crush the rock core in the hole prior to retrieving the core to surface making it difficult to evaluate the quality of the cores. The special core barrel may be needed to crush the rock cores during construction.
- Video inspection of the test caisson is recommended to confirm the quality of the rock socket due to the encountered difficulties of evaluating the quality of the recovered cores in the test caisson. However, if pumping of groundwater to inspect the socket would tend to destabilize the excavation due to pumping of fine sand through the fractured zone, an alternate method to retrieve the intact portions of the socket core should be utilized. This should be combined with maintaining an excess water head inside the inner casing and probing the base of the socket with a weighted steel probe bar after cleaning and immediately before tremie concrete placement.
- The Soilmecc SR-65 or equivalent drill rig is capable of drilling deep caissons to the required depth in a time-efficient manner.
- Tremie placement of concrete will be required due to the large amount of water seepage from the bedrock aquifer.
- The depth to competent bedrock is expected to vary across the site and it should be recognized that the test holes advanced at the bridge abutment and pier locations are more representative of expected ground conditions at those locations.

The geotechnical report dated March 2013 should be consulted for additional information and full geotechnical recommendations. We trust the information provided herein is sufficient for your purposes.

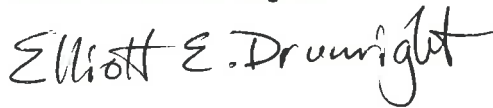
Please don't hesitate to contact me should you have any questions or concerns.

Submitted by:

Reviewed by:



Zeyad Shukri, M.Sc
Senior Geotechnical Engineer



Elliott E. Drumright, P.E.
Associate Engineer



Patrick C. Chang, P.E., P.Eng.
Senior Project Engineer

Appendix A

Figure 1 / Logs

P:\60273041\000-CADD\02-SHEETS\B\60273041-20-SHT-B-002_RX.dwg

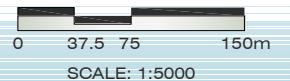


AECOM



**PLESSIS
UNDERPASS STUDY**

Testhole Location Plan



B-002

AECOM Canada Ltd.

GENERAL STATEMENT

NORMAL VARIABILITY OF SUBSURFACE CONDITIONS

The scope of the investigation presented herein is limited to an investigation of the subsurface conditions as to suitability for the proposed project. This report has been prepared to aid in the evaluation of the site and to assist the engineer in the design of the facilities. Our description of the project represents our understanding of the significant aspects of the project relevant to the design and construction of earth work, foundations and similar. In the event of any changes in the basic design or location of the structures as outlined in this report or plan, we should be given the opportunity to review the changes and to modify or reaffirm in writing the conclusions and recommendations of this report.

The analysis and recommendations presented in this report are based on the data obtained from the borings and test pit excavations made at the locations indicated on the site plans and from other information discussed herein. This report is based on the assumption that the subsurface conditions everywhere are not significantly different from those disclosed by the borings and excavations. However, variations in soil conditions may exist between the excavations and, also, general groundwater levels and conditions may fluctuate from time to time. The nature and extent of the variations may not become evident until construction. If subsurface conditions differ from those encountered in the exploratory borings and excavations, are observed or encountered during construction, or appear to be present beneath or beyond excavations, we should be advised at once so that we can observe and review these conditions and reconsider our recommendations where necessary.

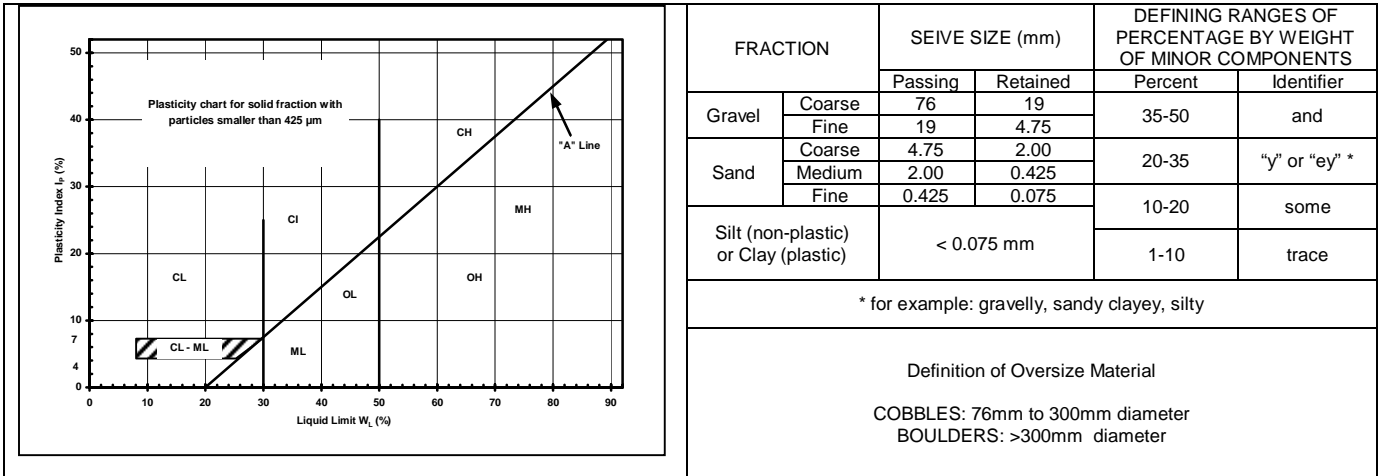
Since it is possible for conditions to vary from those assumed in the analysis and upon which our conclusions and recommendations are based, a contingency fund should be included in the construction budget to allow for the possibility of variations which may result in modification of the design and construction procedures.

In order to observe compliance with the design concepts, specifications or recommendations and to allow design changes in the event that subsurface conditions differ from those anticipated, we recommend that all construction operations dealing with earth work and the foundations be observed by an experienced soils engineer. We can be retained to provide these services for you during construction. In addition, we can be retained to review the plans and specifications that have been prepared to check for substantial conformance with the conclusions and recommendations contained in our report.

EXPLANATION OF FIELD & LABORATORY TEST DATA

Description			AECOM Log Symbols	USCS Classification	Laboratory Classification Criteria				
					Fines (%)	Grading	Plasticity	Notes	
COARSE GRAINED SOILS	GRAVELS (More than 50% of coarse fraction of gravel size)	CLEAN GRAVELS (Little or no fines)	Well graded gravels, sandy gravels, with little or no fines		GW	0-5	$C_u > 4$ $1 < C_c < 3$	Dual symbols if 5-12% fines. Dual symbols if above "A" line and $4 < W_p < 7$ $C_u = \frac{D_{60}}{D_{10}}$ $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$	
			Poorly graded gravels, sandy gravels, with little or no fines		GP	0-5	Not satisfying GW requirements		
		DIRTY GRAVELS (With some fines)	Silty gravels, silty sandy gravels		GM	> 12			Atterberg limits below "A" line or $W_p < 4$
			Clayey gravels, clayey sandy gravels		GC	> 12			Atterberg limits above "A" line or $W_p < 7$
	SANDS (More than 50% of coarse fraction of sand size)	CLEAN SANDS (Little or no fines)	Well graded sands, gravelly sands, with little or no fines		SW	0-5	$C_u > 6$ $1 < C_c < 3$		
			Poorly graded sands, gravelly sands, with little or no fines		SP	0-5	Not satisfying SW requirements		
		DIRTY SANDS (With some fines)	Silty sands, sand-silt mixtures		SM	> 12			Atterberg limits below "A" line or $W_p < 4$
			Clayey sands, sand-clay mixtures		SC	> 12			Atterberg limits above "A" line or $W_p < 7$
FINE GRAINED SOILS	SILTS (Below 'A' line negligible organic content)	$W_L < 50$	Inorganic silts, silty or clayey fine sands, with slight plasticity		ML		Classification is Based upon Plasticity Chart		
		$W_L > 50$	Inorganic silts of high plasticity		MH				
	CLAYS (Above 'A' line negligible organic content)	$W_L < 30$	Inorganic clays, silty clays, sandy clays of low plasticity, lean clays		CL				
		$30 < W_L < 50$	Inorganic clays and silty clays of medium plasticity		CI				
		$W_L > 50$	Inorganic clays of high plasticity, fat clays		CH				
	ORGANIC SILTS & CLAYS (Below 'A' line)	$W_L < 50$	Organic silts and organic silty clays of low plasticity		OL				
		$W_L > 50$	Organic clays of high plasticity		OH				
	HIGHLY ORGANIC SOILS		Peat and other highly organic soils		Pt	Von Post Classification Limit		Strong colour or odour, and often fibrous texture	
	Asphalt		Till			AECOM			
	Concrete		Bedrock (Undifferentiated)						
	Fill		Bedrock (Limestone)						

When the above classification terms are used in this report or test hole logs, the designated fractions may be visually estimated and not measured.



LEGEND OF SYMBOLS

Laboratory and field tests are identified as follows:

- q_u - undrained shear strength (kPa) derived from unconfined compression testing.
- T_v - undrained shear strength (kPa) measured using a torvane
- pp - undrained shear strength (kPa) measured using a pocket penetrometer.
- L_v - undrained shear strength (kPa) measured using a lab vane.
- F_v - undrained shear strength (kPa) measured using a field vane.
- γ - bulk unit weight (kN/m^3).
- SPT - Standard Penetration Test. Recorded as number of blows (N) from a 63.5 kg hammer dropped 0.76 m (free fall) which is required to drive a 51 mm O.D. Raymond type sampler 0.30 m into the soil.
- DPPT - Drive Point Pentrometer Test. Recorded as number of blows from a 63.5 kg hammer dropped 0.76 m (free fall) which is required to drive a 50 mm drive point 0.30 m into the soil.
- w - moisture content (W_L, W_P)

The undrained shear strength (S_u) of a cohesive soil can be related to its consistency as follows:

S_u (kPa)	CONSISTENCY
<12	very soft
12 – 25	soft
25 – 50	medium or firm
50 – 100	stiff
100 – 200	very stiff
200	hard

The resistance (N) of a non-cohesive soil can be related to compactness condition as follows

N – BLOWS/0.30 m	COMPACTNESS
0 - 4	very loose
4 - 10	loose
10 - 30	compact
30 - 50	dense
50	very dense

PROJECT: Plessis Road Underpass		CLIENT: City of Winnipeg		TESTHOLE NO: Test Caisson		
LOCATION: Plessis South Bound/CN Rail Intersection, West of Sidewalk				PROJECT NO.: 60273041		
CONTRACTOR: Subterranean (Manitoba) LTD.		METHOD: Track Mounted Soilmec SR-65		ELEVATION (m): 232.50		
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
BACKFILL TYPE	BENTONITE	GRAVEL	SLOUGH	GROUT	CUTTINGS	SAND

DEPTH (m)	SOIL SYMBOL	BACKFILL DETAILS	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION (m)
							* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ⊕ Field Vane ⊕ (kPa)				
0			CLAY - brown, moist, stiff - high plasticity, silt lenses									232
1												231
2												230
3												229
4			- greyish brown below 3.66 m									228
5												227
6			- grey, soft to firm below 5.49 m									226
7												225
8												224
9												223
10												222
11												221
12												220
13												219
14												218
15												218

LOG OF TEST HOLE TEST CAISSON LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/17



LOGGED BY: Sam O.	COMPLETION DEPTH: 23.93 m
REVIEWED BY: Zeyad Shukri	COMPLETION DATE: 13/7/9
PROJECT ENGINEER: Zeyad Shukri	Page 1 of 2

PROJECT: Plessis Road Underpass		CLIENT: City of Winnipeg		TESTHOLE NO: Test Caisson		
LOCATION: Plessis South Bound/CN Rail Intersection, West of Sidewalk				PROJECT NO.: 60273041		
CONTRACTOR: Subterranean (Manitoba) LTD.		METHOD: Track Mounted Soilmec SR-65		ELEVATION (m): 232.50		
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
BACKFILL TYPE	BENTONITE	GRAVEL	SLOUGH	GROUT	CUTTINGS	SAND

DEPTH (m)	SOIL SYMBOL	BACKFILL DETAILS	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION (m)
							* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ⊗ Field Vane ⊗ (kPa)				
15												217
16												216
17			- wet below 16.76 m									215
18			- fractured rock, cobbles and boulders below 17.53 m									214
19			LIMESTONE (Bedrock) - weathered - light grey to white - fine to medium grained, no foliations - R2, weak strength rock - suspected cavity (< 0.5 m) - fractured to 20.9 m below ground surface									213
20												212
21												211
22			- competent rock at 21.6 m below ground surface, R3 (medium strong) - light grey to white - fine to medium grained, no foliations - Rough planar joints									210
23												209
24			END OF TEST CAISSON AT 23.9 m IN BEDROCK									208
25			Notes: 1. bedrock encountered at 17.8 m below ground surface. 2. Seepage observed at 16.7 m below ground surface, static water level at 10.7 m below ground surface. 3. 0.76 m diameter coring below 17.8 m. 4. Test caisson backfilled with concrete up to 11.4 m, plugged with stabilized fill from 11.4 to ground surface.									207
26												206
27												205
28												204
29												203
30												203

LOG OF TEST HOLE TEST CAISSON LOGS-PRU-60273041 - UPDATED.GPJ UMA WINN.GDT 13/10/17



LOGGED BY: Sam O.	COMPLETION DEPTH: 23.93 m
REVIEWED BY: Zeyad Shukri	COMPLETION DATE: 13/7/9
PROJECT ENGINEER: Zeyad Shukri	Page 2 of 2

Memorandum

To	Bob Paetsch	Page	1
CC	Brent Knezacek		
Subject	CN Railway Detour Stability Analysis		
From	Omer Eissa		
Date	April 22 th , 2013	Project Number	60273041

Introduction

AECOM was retained by the City of Winnipeg to provide preliminary design including geotechnical engineering services for the proposed Plessis Road Underpass in Winnipeg, Manitoba. As part of the works, the CN railway tracks crossing Plessis Road will have to be relocated south of the existing crossing for the duration of the bridge construction. The location of the railway detour (shoofly) in relation to the underpass and bridge structure is shown in the drawing labelled Draft CR-01 attached in Appendix A. This memorandum summarizes the stability analysis results for the proposed CN railway detour embankment at the location of the bridge construction.

The proposed CN railway embankment is seven (7) meters wide at the top of the embankment and consists of railway ties over a ballast layer of 0.47 m thickness. A sub-ballast layer lies under the ballast layer and extends from a thickness of 0.3 m at the centre of the embankment with a cross fall of 1:40 towards the edges of the embankment. The shoofly is expected to perform as a temporary detour for the duration of the bridge construction. The shoofly embankment is located approximately 17 m measured from the centreline of the south existing CN track to the centreline of the north detour track. Proposed shoofly plan and cross-sections are shown in Figure CS-16 attached in Appendix A.

Stability Modelling

The proposed shoofly embankment shown in Figure CS-16 was modelled using the soil strength parameters presented in Table -01 below.

Table 01: Strength Parameters for Slope Stability Analysis

Material	Unit Weight (kN/m)	Cohesion (kPa)	Angle of Internal Friction (°)	Modulus of Elasticity (kPa)	Poisson's Ratio
Ballast	20	0	40	115,000	0.33
Sub-ballast	20	0	40	115,000	0.33
Granular Fill	19	0	38	100,000	0.33
Native Clay	17	5	17	6000	0.4

The analysis was conducted using the Sigma/W and Slope/W Geo Studio software. A stepped analysis showing each stage of the construction was modelled in Sigma/W. The purpose of a stepped or (treed) analysis is to import the soil stress state from the initial in-situ model and recalculate the soil stress redistribution and pore-water response for each construction stage. The embankment loading was modelled according to the CN memo dated 2011, November 22, titled “Design Criteria for the Shoring Walls submitted by the Consultant”. The surcharge due to the Cooper-E90 loading as per AREMA-2010 was modelled as a 90 kips axle load at 5 ft spacing over an 8-ft-long tie for a resulting surcharge of approximately 110 kPa. A Slope/W stability analysis was conducted for the critical stage of construction where the detour embankment is loaded with Cooper E90 train loads nearby the bridge excavation (Case-05e). Table-02 below lists and describes the cases of stability modelling representing the stages of embankment and bridge construction.

Water conditions were modelled in the in-situ Sigma/W model based on the site groundwater monitoring results. The groundwater table measured on site between December 2012, to April 2013 fluctuated between elevations 226.5 to 228.2 m. Groundwater was modelled in the in-situ model at elevation 229 m.

Table 02: List and Description of Modelling Stages

Analysis ID	Analysis Type	Construction Condition
Case-01a	Sigma/W- In Situ	Initial Condition
Case-02b	Sigma/W- Stress Redistribution	Detour Excavation
Case-03c	Sigma/W- Stress Redistribution	Embankment fill Placement
Case-04d	Sigma/W- Stress Redistribution	Bridge Excavation + Embankment Loading
Case- 05e	Slope/W – Stress Imported Analysis	Slope Stability with imported stress conditions from Case-04d
Case-02	Slope/W – Morgenstern-Price Analysis	Slope Stability without imported stress conditions

Analysis results are presented graphically in Figures 01- 06 attached in Appendix A.

Analysis Results

An adequate factor of safety (FS) against slope instability must be achieved for short term and long term conditions of the detour embankment. A design factor of safety of at least 1.5 is considered satisfactory for the long term condition of an unloaded embankment. For the case of the loaded embankment with one or two train loads, a factor of safety of at least 1.3 is considered adequate.

The embankment as shown in Figure CS16 did not meet the design target factors of safety against slope instability. A well-compacted granular layer of 1.0 m thickness was therefore incorporated into the embankment between the sub-ballast and subgrade layers. The granular fill can be regarded as an extension of the sub-ballast layer with respect to material type and compaction criteria. The purpose of this layer is to replace weaker subgrade material as well as function as a pad to distribute the embankment load onto a larger area of the subgrade. Factors of safety for the embankment after extending the sub-ballast layer, i.e.: inclusion of the granular layer, are presented in Table-03. Figures outlining individual analysis results are attached in Appendix A.

Table-03 Factor of Safety Against Slope Instability

Case	Loading Conditions	Computed F.S	Design F.S
Case-05e	North track loaded	1.36	1.3
	South track loaded	1.63	1.3
	Both tracks loaded	1.35	1.3
	No train loads	1.86	1.5
Case-02	North track loaded	1.31	1.3
	South track loaded	1.59	1.3
	Both tracks loaded	1.31	1.3
	No train loads	1.97	1.5

We trust the information provided is sufficient for your purposes. Please don't hesitate to contact the undersigned should you have any questions or concerns.

Prepared by,



Omer Eissa, P.Eng
Geotechnical Engineer

Reviewed by,

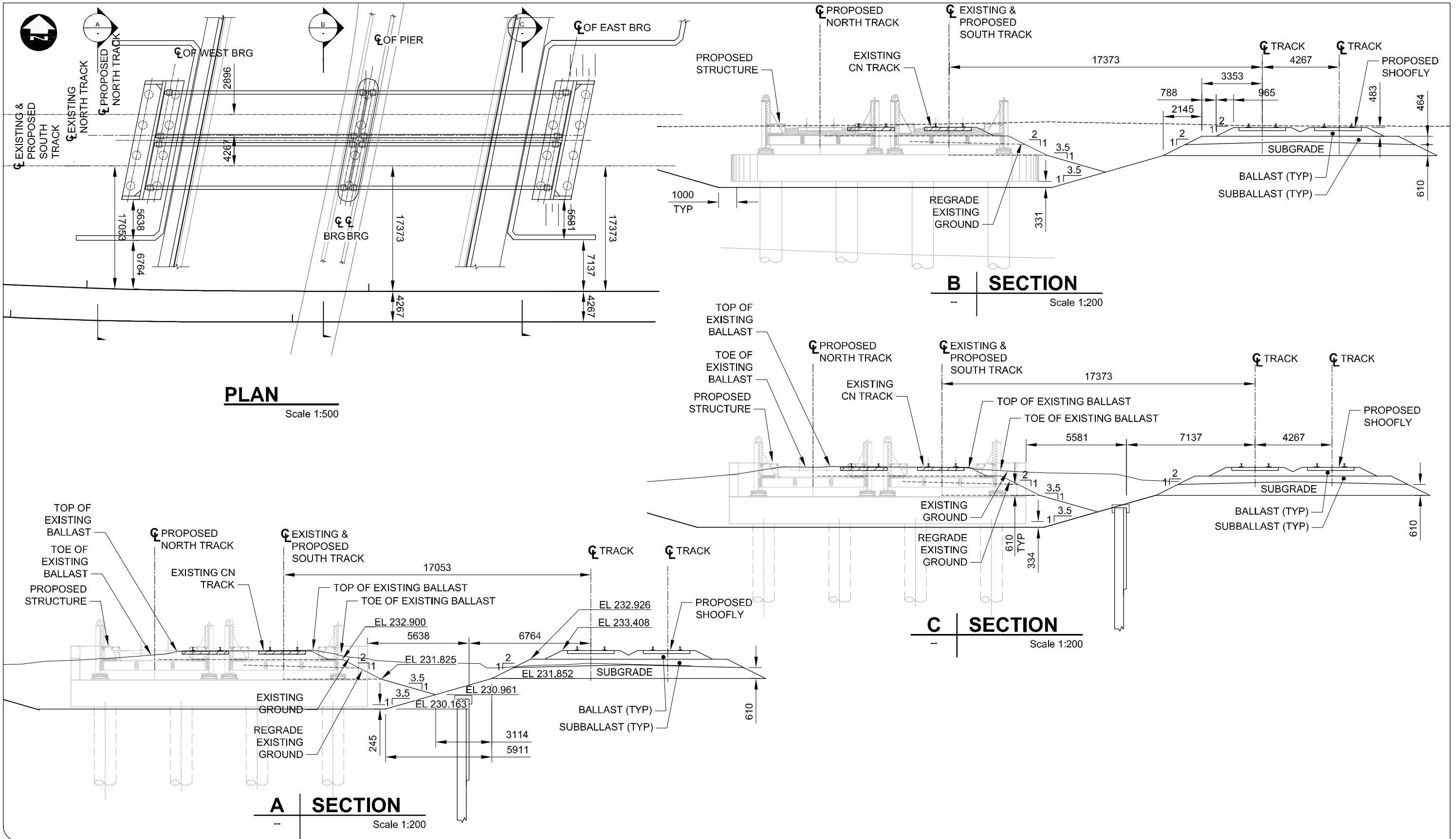


Zeyad Shukri
Senior Geotechnical Engineer

Appendix A

Figures

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AECOM

**DILLON
CONSULTING**

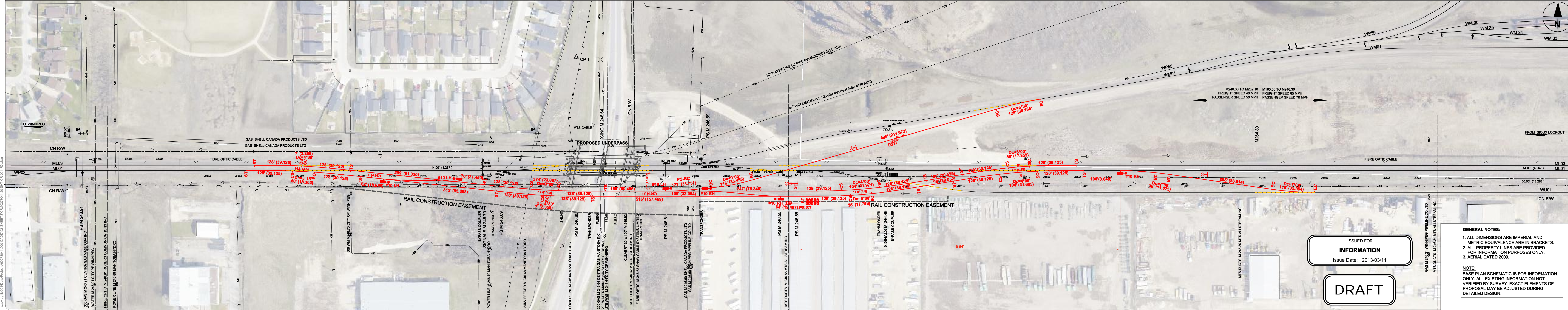
Winnipeg

**PLESSIS
UNDERPASS STUDY**

**2 SPAN SINGLE TRACK TPG OPTION
SOUTH TRACK ALIGNMENT**

FIGURE CS16

- CROSSING PLANKS
- CENTERLINE PROP TRACK
- CP 000 CONTROL POINT
- RAILWAY RW
- EXISTING DITCH FLOW ARROW
- EXISTING CULVERT
- POWER SWITCH
- PROPOSED POWER SWITCH
- OVERHEAD POWER LINE WITH POLE
- OVERHEAD CNT LINE WITH POLE
- BLOWER
- RAIL REMOVE /REALIGN



ISSUED FOR
INFORMATION
Issue Date: 2013/03/11

DRAFT

- GENERAL NOTES:**
1. ALL DIMENSIONS ARE IMPERIAL AND METRIC EQUIVALENCE ARE IN BRACKETS.
 2. ALL PROPERTY LINES ARE PROVIDED FOR INFORMATION PURPOSES ONLY.
 3. AERIAL DATED 2009.

NOTE:
BASE PLAN SCHEMATIC IS FOR INFORMATION ONLY. ALL EXISTING INFORMATION NOT VERIFIED BY SURVEY. EXACT ELEMENTS OF PROPOSAL MAY BE ADJUSTED DURING DETAILED DESIGN.

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Figure 1:

Name: Sigma - Insitu
Kind: SIGMA/W
Method: Insitu

Name: Clay
Model: Linear Elastic
Effective Young's Modulus (E'): 6000 kPa
Poisson's Ratio: 0.4
Insitu Ko: 0.66666667
Unit Weight: 17 kN/m³

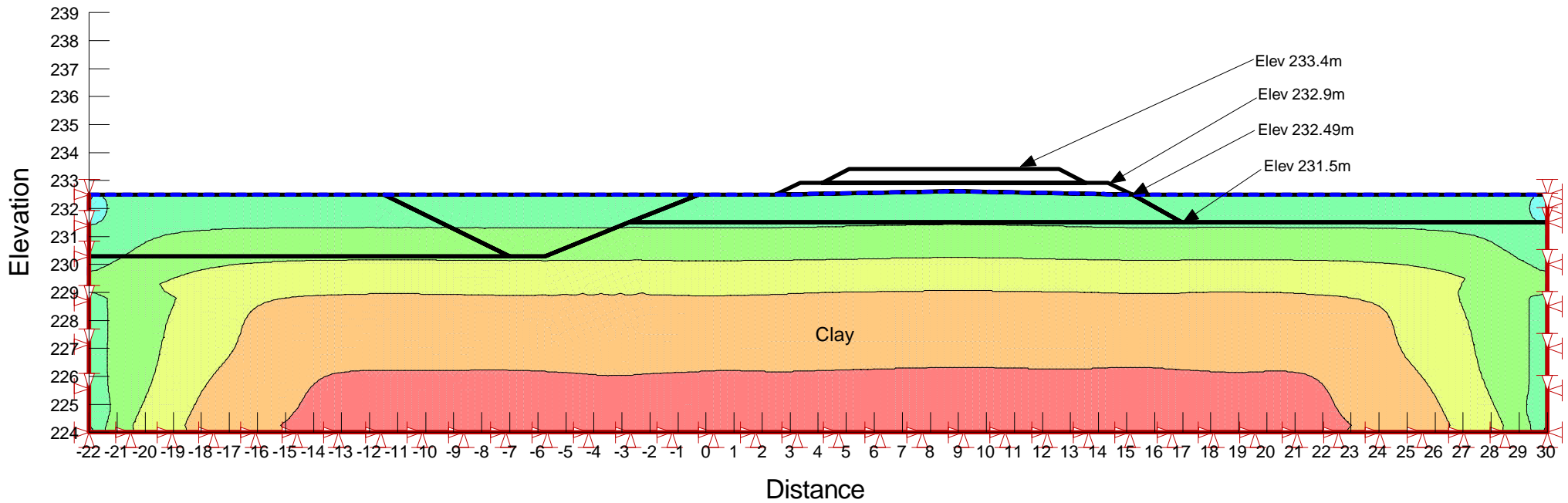


Figure 2:

Name: ShooFly Excavation
Kind: SIGMA/W
Method: Load/Deformation

Name: Clay
Model: Linear Elastic
Effective Young's Modulus (E'): 6000 kPa
Poisson's Ratio: 0.4
Unit Weight: 17 kN/m³

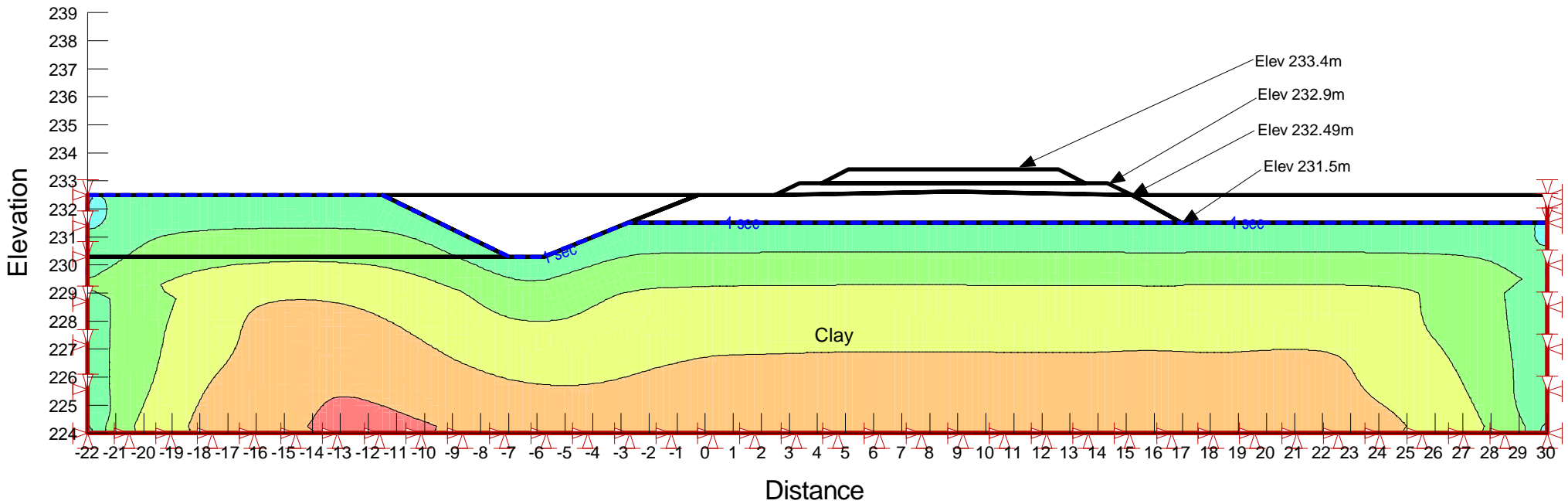


Figure 3:

Name: Embankment Fill
Kind: SIGMA/W
Method: Load/Deformation

Name: Clay
Model: Linear Elastic
Effective Young's Modulus (E'): 6000 kPa
Poisson's Ratio: 0.4
Unit Weight: 17 kN/m³

Name: Ballast
Model: Linear Elastic
Effective Young's Modulus (E'): 120000 kPa
Poisson's Ratio: 0.334
Unit Weight: 20 kN/m³

Name: Granular
Model: Linear Elastic
Effective Young's Modulus (E'): 100000 kPa
Poisson's Ratio: 0.334
Unit Weight: 19 kN/m³

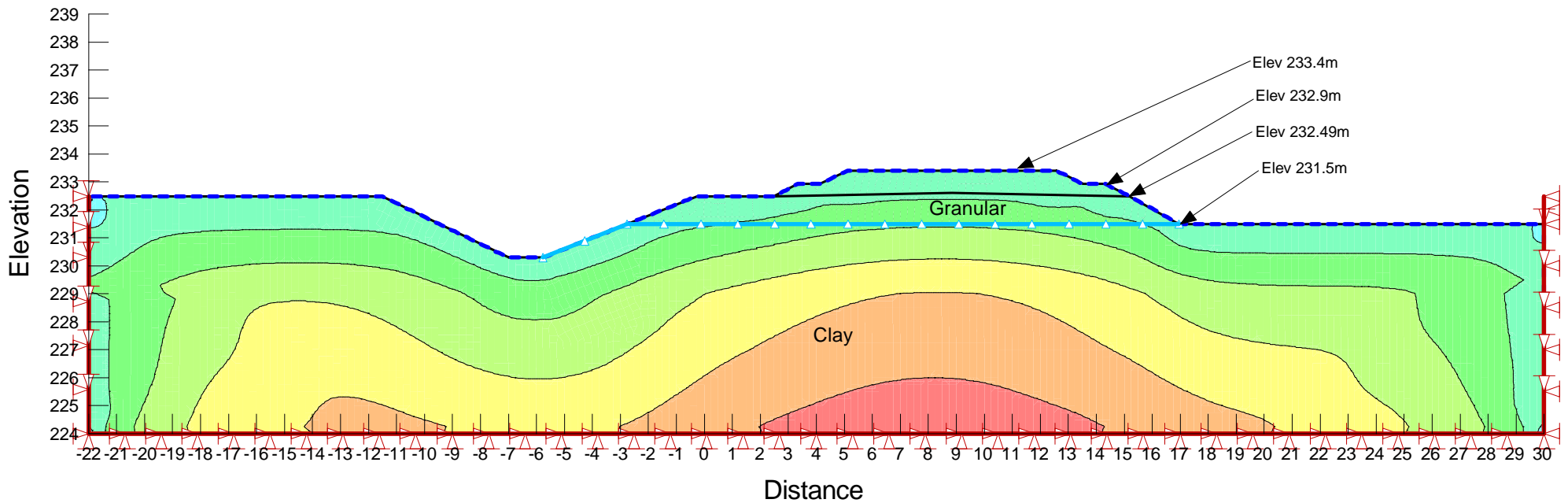


Figure 4:

Name: Bridge Excavation and Surcharge Loading
Kind: SIGMA/W
Method: Load/Deformation
Load Condition: Two Surcharge loads of 110 kPa

Name: Clay
Model: Linear Elastic
Effective Young's Modulus (E'): 6000 kPa
Poisson's Ratio: 0.4
Unit Weight: 17 kN/m³

Name: Ballast
Model: Linear Elastic
Effective Young's Modulus (E'): 120000 kPa
Poisson's Ratio: 0.334
Unit Weight: 20 kN/m³

Name: Granular
Model: Linear Elastic
Effective Young's Modulus (E'): 100000 kPa
Poisson's Ratio: 0.334
Unit Weight: 19 kN/m³

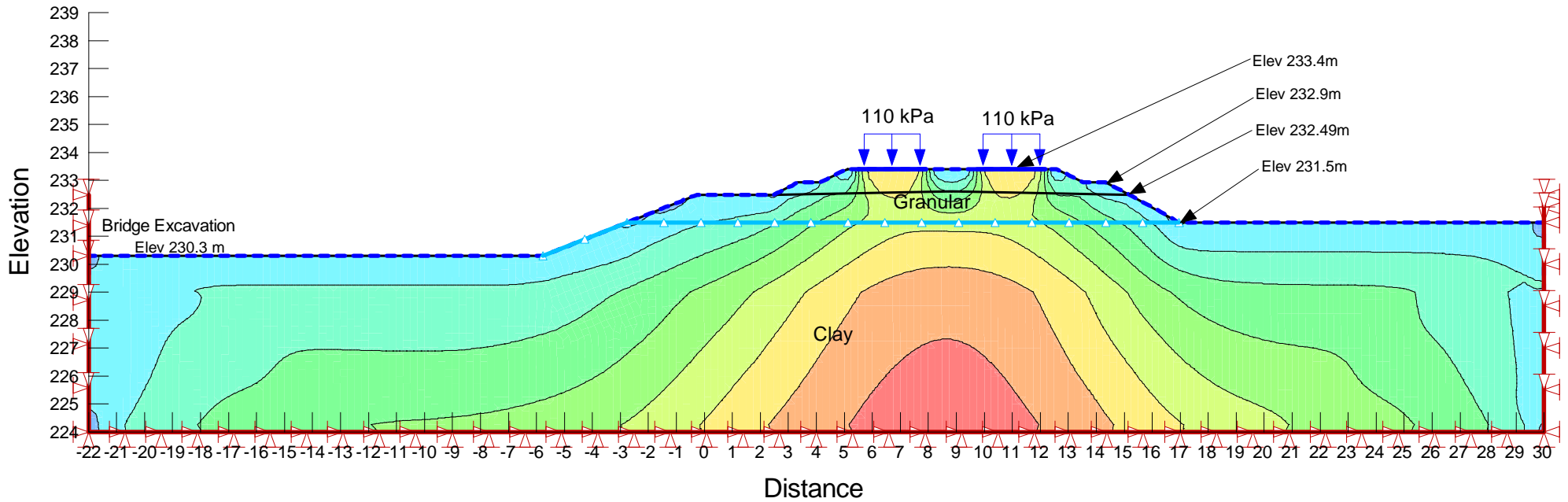


Figure 5:

Name: Bridge Excavation Stability Analysis

Kind: SLOPE/W

Method: SIGMA/W Stress

Loading Condition: Surcharge loads of 110 kPa on each Track

Unit weight: 17 kN/m³

Cohesion: 5 kPa

Phi: 17 °

Phi-B: 0 °

Name: Ballast

Model: Mohr-Coulomb

Unit Weight: 20 kN/m³

Cohesion: 0 kPa

Phi: 40 °

Phi-B: 0 °

Name: Granular

Model: Mohr-Coulomb

Unit Weight: 19 kN/m³

Cohesion: 0 kPa

Phi: 38 °

Phi-B: 0 °

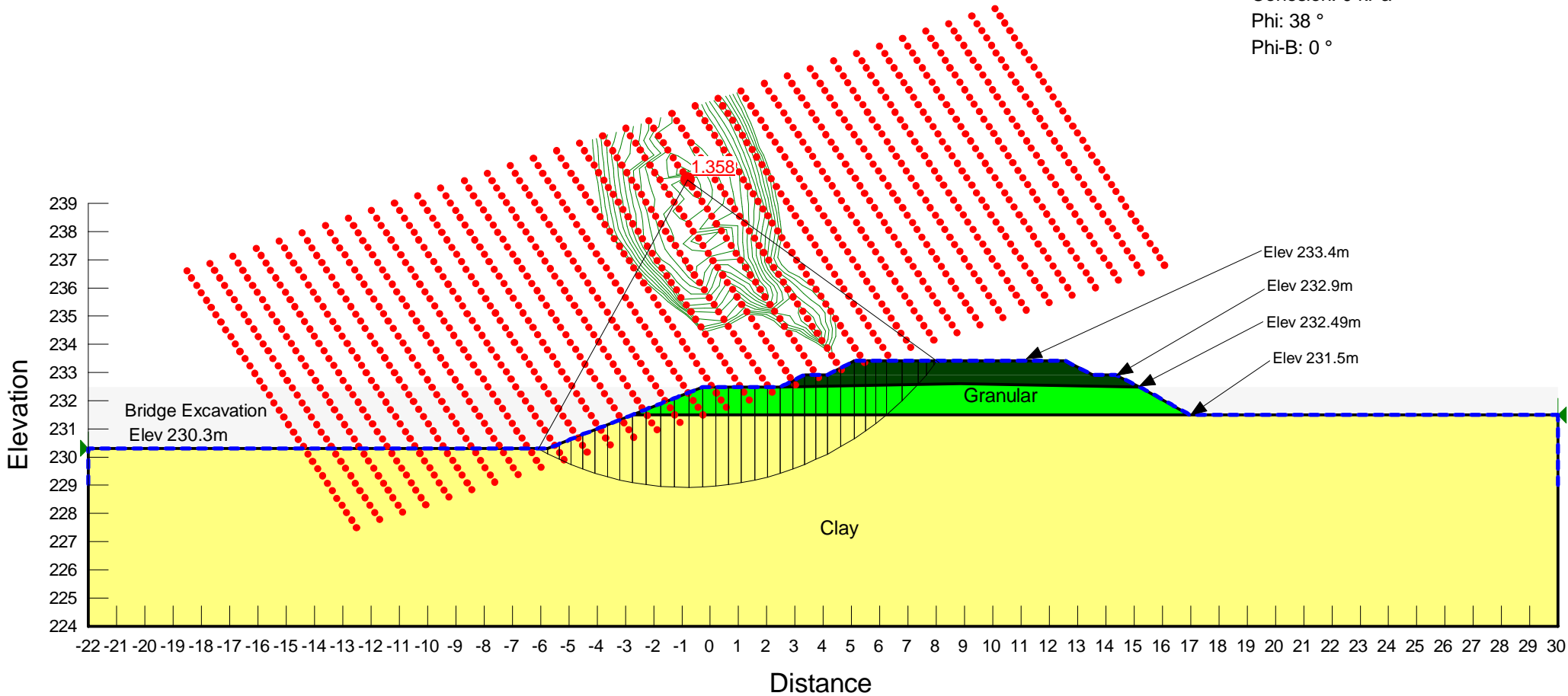


Figure 6:

Name: Stability Analysis

Kind: SLOPE/W

Method: Morgenstern-Price

Loading Condition: Surcharge loads of 110 kPa on each Track

Unit Weight: 17 kN/m³

Cohesion: 5 kPa

Phi: 17 °

Phi-B: 0 °

Piezometric Line: 1

Name: Ballast

Model: Mohr-Coulomb

Unit Weight: 20 kN/m³

Cohesion: 0 kPa

Phi: 40 °

Phi-B: 0 °

Piezometric Line: 1

Name: Granular

Model: Mohr-Coulomb

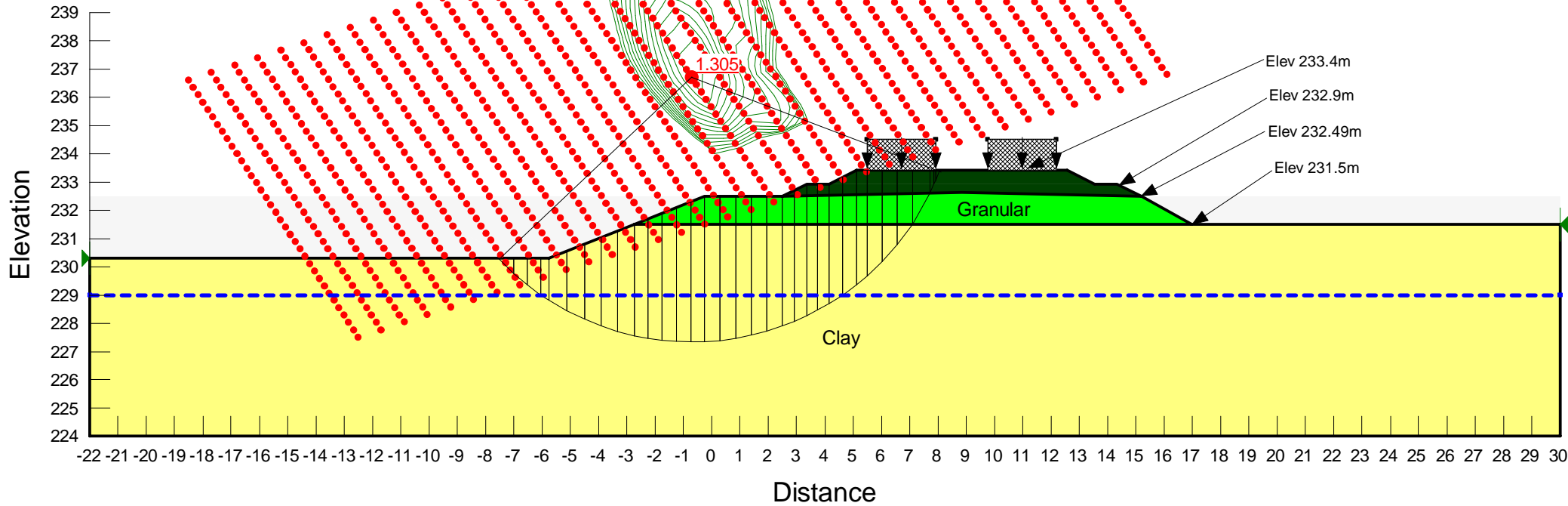
Unit Weight: 19 kN/m³

Cohesion: 0 kPa

Phi: 38 °

Phi-B: 0 °

Piezometric Line: 1



Memorandum

To	Brent Knezacek	Page	1
CC	Tanya Worms		
Subject	CN Railway Detour Stability Analysis		
From	Mustafa Alkiki		
Date	October 31, 2013	Project Number	60273041 (404.19.2)

Introduction

AECOM was retained by the City of Winnipeg to provide a detailed design including geotechnical engineering services for the proposed Plessis Road Underpass in Winnipeg, Manitoba. As part of the project, the existing CN railway tracks crossing Plessis Road will have to be relocated south of the existing crossing for the duration of the bridge construction. The location of the railway detour (shoofly) in relation to the underpass and bridge structure is shown in the attached drawing Number CS-0005, Appendix A. In addition, we understand that excavation work will be carried out at the junction between the railway detour and Plessis Road. This memorandum summarizes the stability analysis results for the proposed CN railway detour embankment at the bridge location and further at the intersection with Plessis Road.

The proposed CN railway embankment is approximately 7.46 meters wide at the top of the embankment and consists of railway ties over a ballast layer of 0.48 m thickness. A sub-ballast layer lies under the ballast layer and extends from a thickness of 0.3 m at the centre of the embankment with a cross fall of 1:40 towards the edges of the embankment. A well-compacted granular layer of 1.0 m thickness lies between the sub-ballast and subgrade layers. The shoofly is expected to perform as a temporary detour for the duration of the bridge construction. The shoofly embankment is located approximately 17 m from the centerline of the south existing CN track to the centerline of the north detour track. The proposed shoofly plan and cross-sections are shown in Figures CS-0004 and CS-0005, attached in Appendix A.

Stability Modelling

The proposed shoofly embankment shown in Figures CS-004 and CS-0005 was modelled using the soil strength parameters presented in Table 01, below.

Table 01: Strength Parameters for Slope Stability Analysis

Material	Unit Weight (kN/m)	Cohesion (kPa)	Angle of Internal Friction (°)	Modulus of Elasticity (kPa)	Poisson's Ratio
Ballast	20	0	40	120,000	0.25
Sub-ballast	20	0	40	120,000	0.25
Granular Fill	19	0	38	100,000	0.33
Native Clay	17	5	18	6,000	0.4

The analysis was conducted using Sigma/W and Slope/W Geo Studio software. A stepped analysis showing each stage of the construction was modelled in Sigma/W. The purpose of a stepped (or treed) analysis is to import the soil stress state from the initial in-situ model and recalculate the soil stress redistribution and pore-water response for each construction stage. The embankment loading was modelled according to the CN memorandum dated November 22, 2011 and titled "Design Criteria for the Shoring Walls submitted by the Consultant". The surcharge due to the Cooper-E90 loading as per AREMA-2010 was modelled as a 90 kips axle load at 5 ft spacing over an 8-ft-long tie for a resulting surcharge of approximately 110 kPa. A Slope/W stability analysis was conducted for the critical stage of construction where the detour embankment is loaded with Cooper E90 train loads nearby the bridge excavation. Three cases were considered in the analysis:

- Case 1: A maximum excavation depth up to +230 m was modeled with side slope of 2:1 (north side excavation).
- Case 2: A maximum excavation depth up to +226 m and side slope of 4:1 (north side excavation).
- Case 3: A maximum excavation depth up to +228.5 m and side slope of 4:1 (south side excavation).

Table 02, below, lists and describes the cases of stability modelling representing the stages of embankment and bridge construction.

Water conditions were modelled in the in-situ Sigma/W model based on the site groundwater monitoring results. The groundwater table measured on-site between December 2012 and June 2013 fluctuated between elevations of 226.5 to 228.2 m. Groundwater was modelled in the in-situ model at elevation 228 m.

Table 02: List and Description of Modelling Stages

Analysis ID	Analysis Type	Construction Condition
Case-01a	Sigma/W- In Situ	Initial Condition
Case-01b	Sigma/W- Stress Redistribution	Detour Excavation
Case-01c	Sigma/W- Stress Redistribution	Embankment Fill Placement
Case-01d	Sigma/W- Stress Redistribution	Bridge Excavation + Embankment Loading
Case- 01e	Slope/W – Stress Imported Analysis	Slope Stability with Imported Stress Conditions from Case-01d
Case- 01f	Slope/W – Morgenstern-Price Analysis	Slope Stability without Imported Stresses
Case-02a	Sigma/W- Stress Redistribution	Roadside Excavation + Embankment Loading
Case-02b	Slope/W – Stress Imported Analysis	With Imported Stress Conditions from Case-02a
Case-02c	Slope/W – Morgenstern-Price Analysis	Slope Stability without Imported Stresses

Analysis ID	Analysis Type	Construction Condition
Case-03a	Sigma/W- Stress Redistribution	Roadside Excavation + Embankment Loading
Case-03b	Slope/W – Stress Imported Analysis	With Imported Stress Conditions from Case-03a
Case-03c	Slope/W – Morgenstern-Price Analysis	Slope Stability without Imported Stresses

Analysis results are presented graphically in Figures 01 through 012, attached in Appendix A.

Analysis Results

An adequate factor of safety (FS) against slope instability must be achieved for short- and long- term conditions of the detour embankment. A design factor of safety of at least 1.5 is considered satisfactory for the long-term condition of an unloaded embankment. For the case of the loaded embankment with one or two train loads, a factor of safety of at least 1.3 is considered adequate.

For Case 1, the embankment as shown in Figures CS-004 and CS-005 meets the design target factors of safety against slope instability. Stability analysis for Case 2, as shown in Figure 10 in Appendix A, meets the design target factors of safety by utilizing a platform of 7.5 m wide at + 230 m and then excavating with 4:1 slope to the final level of +226 m along Plessis Road. Figure 10 shows the dimensions of the proposed geometry required to fulfill design factors of safety for Case 2. Stability analysis for Case 3 revealed that in order to meet the design factor of safety against slope instability, a 2.74 m wide buttress should be placed to maintain the native granular soil, and the excavation can be extended with a 4:1 slope to the final level of +228.5 along Plessis Road. Factors of safety for the three cases are presented in Table 03. Figures outlining individual analysis results are attached in Appendix A.

Table 03: Factor of Safety Against Slope Instability

Case	Loading Conditions	Computed F.S	Design F.S	Figure No.
Case-01e	North track loaded	1.32	1.3	-
	South track loaded	1.58	1.3	-
	Both tracks loaded	1.33	1.3	05
	No train loads	1.64	1.5	-
Case-01f	North track loaded	1.31	1.3	-
	South track loaded	1.66	1.3	-
	Both tracks loaded	1.31	1.3	06
	No train loads	1.73	1.5	-
Case-02b	North track loaded	1.38	1.3	-
	South track loaded	1.45	1.3	-
	Both tracks loaded	1.32	1.3	08
	No train loads	1.60	1.5	-
Case-02c	North track loaded	1.35	1.3	-
	South track loaded	1.43	1.3	-
	Both tracks loaded	1.33	1.3	09
	No train loads	1.52	1.5	-
Case-03b	Both tracks loaded	1.33	1.3	11
Case-03c	Both tracks loaded	1.32	1.3	12
	No train loads	1.83	1.5	-

We trust the information provided is sufficient for your purposes. Please don't hesitate to contact the undersigned should you have any questions or concerns.

Prepared by,



Mustafa Alkiki, EIT
 Geotechnical Engineer-In-Training

Reviewed by,



Zeyad Shukri, M.Sc.
 Senior Geotechnical Engineer



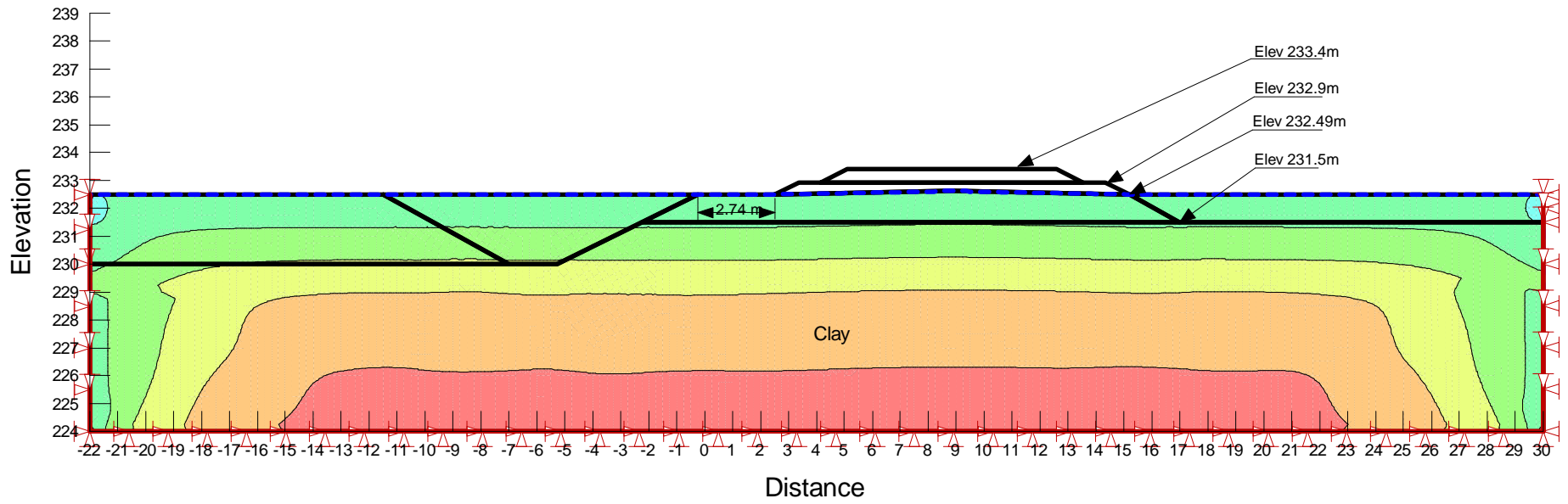
Patrick C. Chang, P.E., P.Eng.
 Senior Project Engineer

Appendix A

Figures

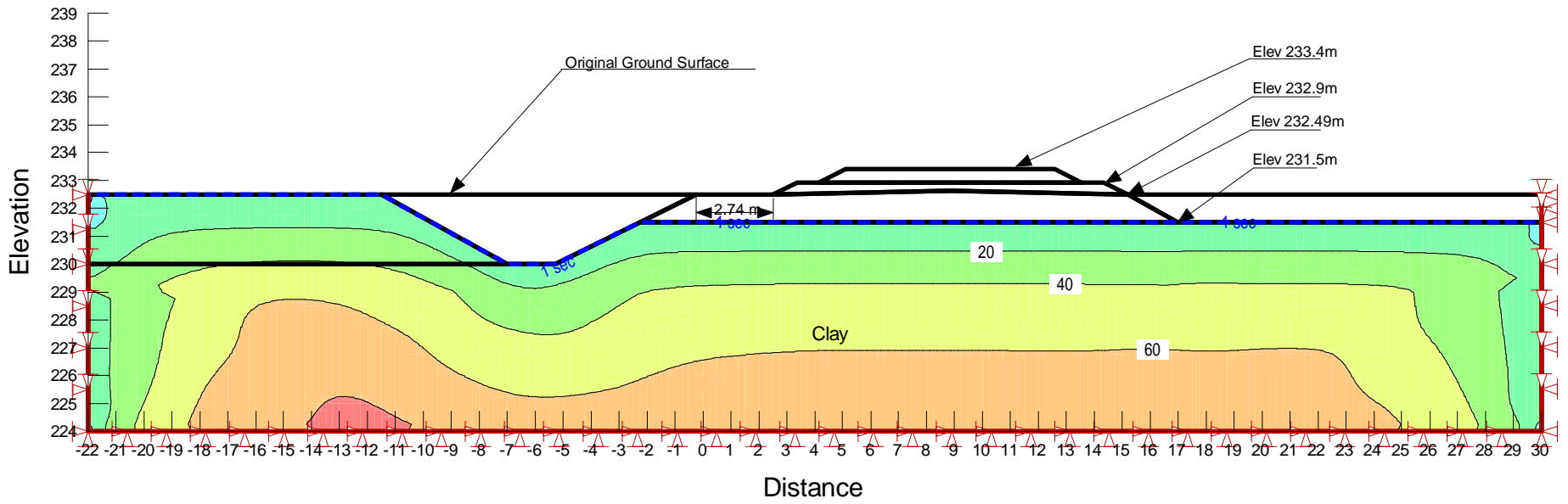
Plessis Rd Underpass
Name: Sigma - In-situ
Method: Method: Insitu
Kind: SIGMA/W
Figure 01: Case 01a

Name: Clay
Model: Linear Elastic
Effective Young's Modulus (E'): 6000 kPa
Poisson's Ratio: 0.4
Insitu Ko: 0.66666667
Unit Weight: 17 kN/m³



Plessis Rd Underpass
Name: ShooFly Excavation
Method: Method: Load/Deformation
Kind: SIGMA/W
Figure 02: Case 01b

Name: Clay
 Model: Linear Elastic
 Effective Young's Modulus (E'): 6000 kPa
 Poisson's Ratio: 0.4
 Unit Weight: 17 kN/m³

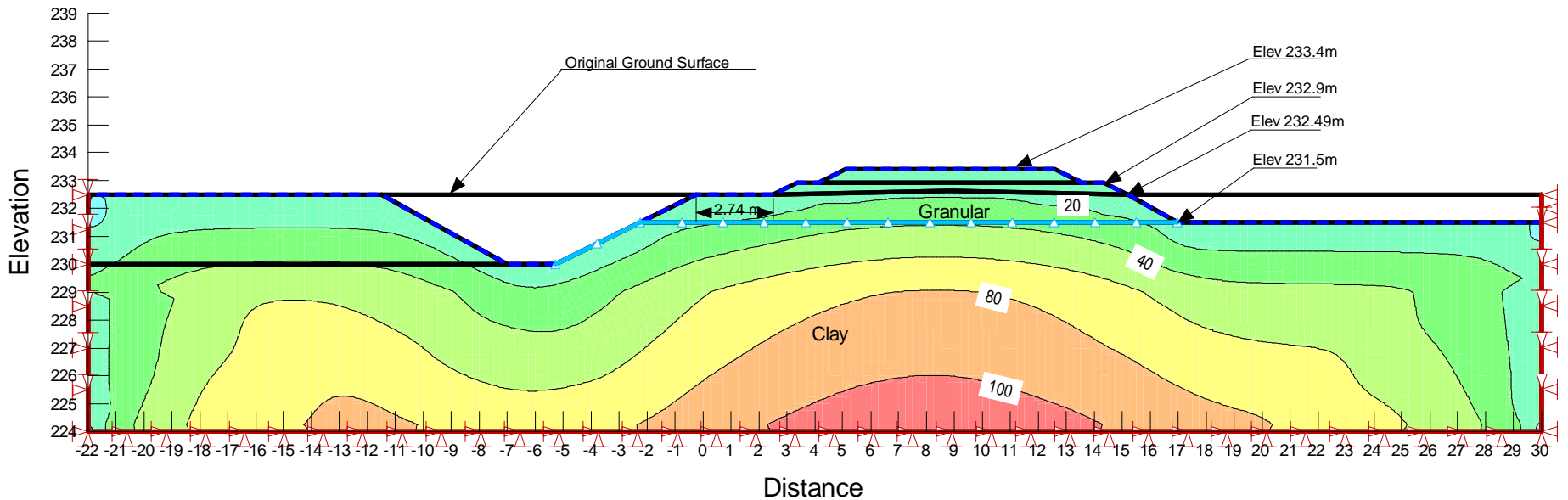


Plessis Rd Underpass
Name: Embankment Fill Placement
Method: Method: Load/Deformation
Kind: SIGMA/W
Figure 03: Case 01c

Name: Clay
 Model: Linear Elastic
 Effective Young's Modulus (E'): 6000 kPa
 Poisson's Ratio: 0.4
 Unit Weight: 17 kN/m³

Name: Ballast
 Model: Linear Elastic
 Effective Young's Modulus (E'): 120000 kPa
 Poisson's Ratio: 0.25
 Unit Weight: 20 kN/m³

Name: Granular
 Model: Linear Elastic
 Effective Young's Modulus (E'): 100000 kPa
 Poisson's Ratio: 0.334
 Unit Weight: 19 kN/m³

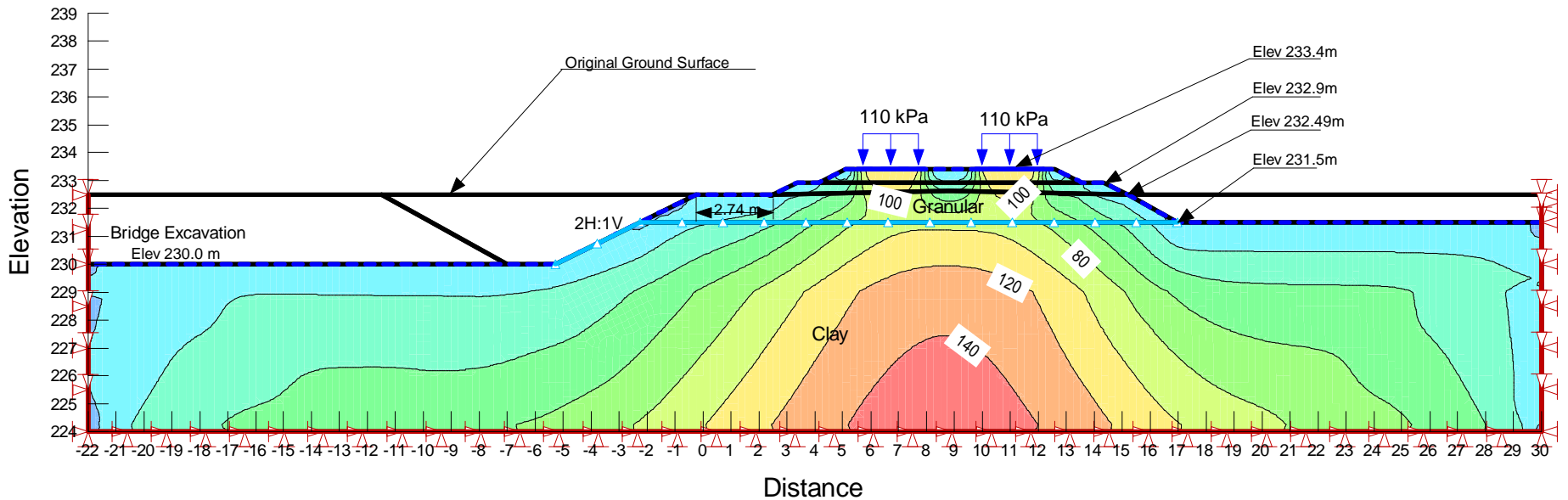


Plessis Rd Underpass
Name: Bridge Excavation and Surcharge Loading
Method: Method: Load/Deformation
Kind: SIGMA/W
Figure 04: Case 01d

Name: Clay
 Model: Linear Elastic
 Effective Young's Modulus (E'): 6000 kPa
 Poisson's Ratio: 0.4
 Unit Weight: 17 kN/m³

Name: Ballast
 Model: Linear Elastic
 Effective Young's Modulus (E'): 120000 kPa
 Poisson's Ratio: 0.25
 Unit Weight: 20 kN/m³

Name: Granular
 Model: Linear Elastic
 Effective Young's Modulus (E'): 100000 kPa
 Poisson's Ratio: 0.334
 Unit Weight: 19 kN/m³

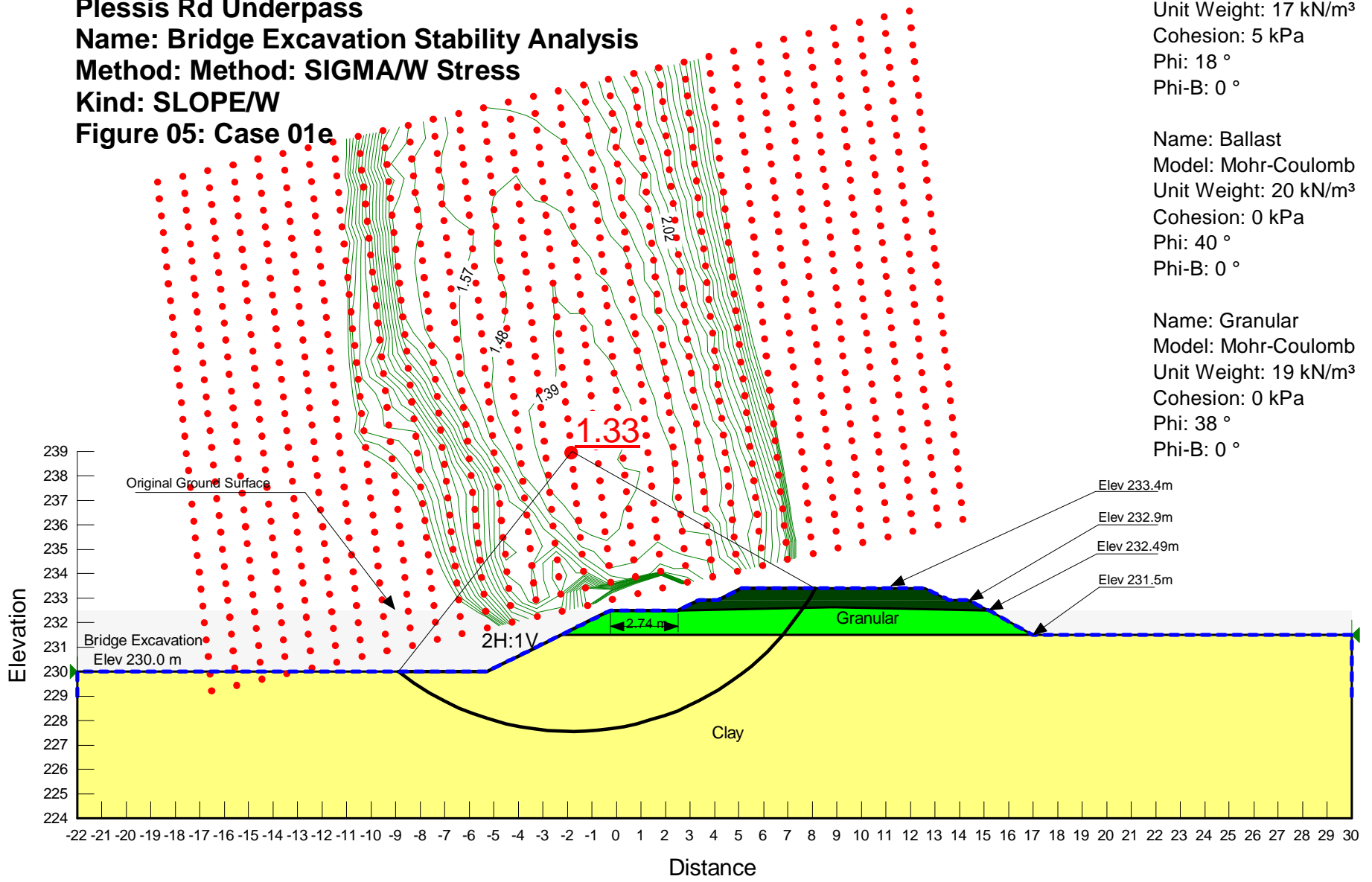


Plessis Rd Underpass
Name: Bridge Excavation Stability Analysis
Method: Method: SIGMA/W Stress
Kind: SLOPE/W
Figure 05: Case 01e

Name: Clay
 Model: Mohr-Coulomb
 Unit Weight: 17 kN/m³
 Cohesion: 5 kPa
 Phi: 18 °
 Phi-B: 0 °

Name: Ballast
 Model: Mohr-Coulomb
 Unit Weight: 20 kN/m³
 Cohesion: 0 kPa
 Phi: 40 °
 Phi-B: 0 °

Name: Granular
 Model: Mohr-Coulomb
 Unit Weight: 19 kN/m³
 Cohesion: 0 kPa
 Phi: 38 °
 Phi-B: 0 °

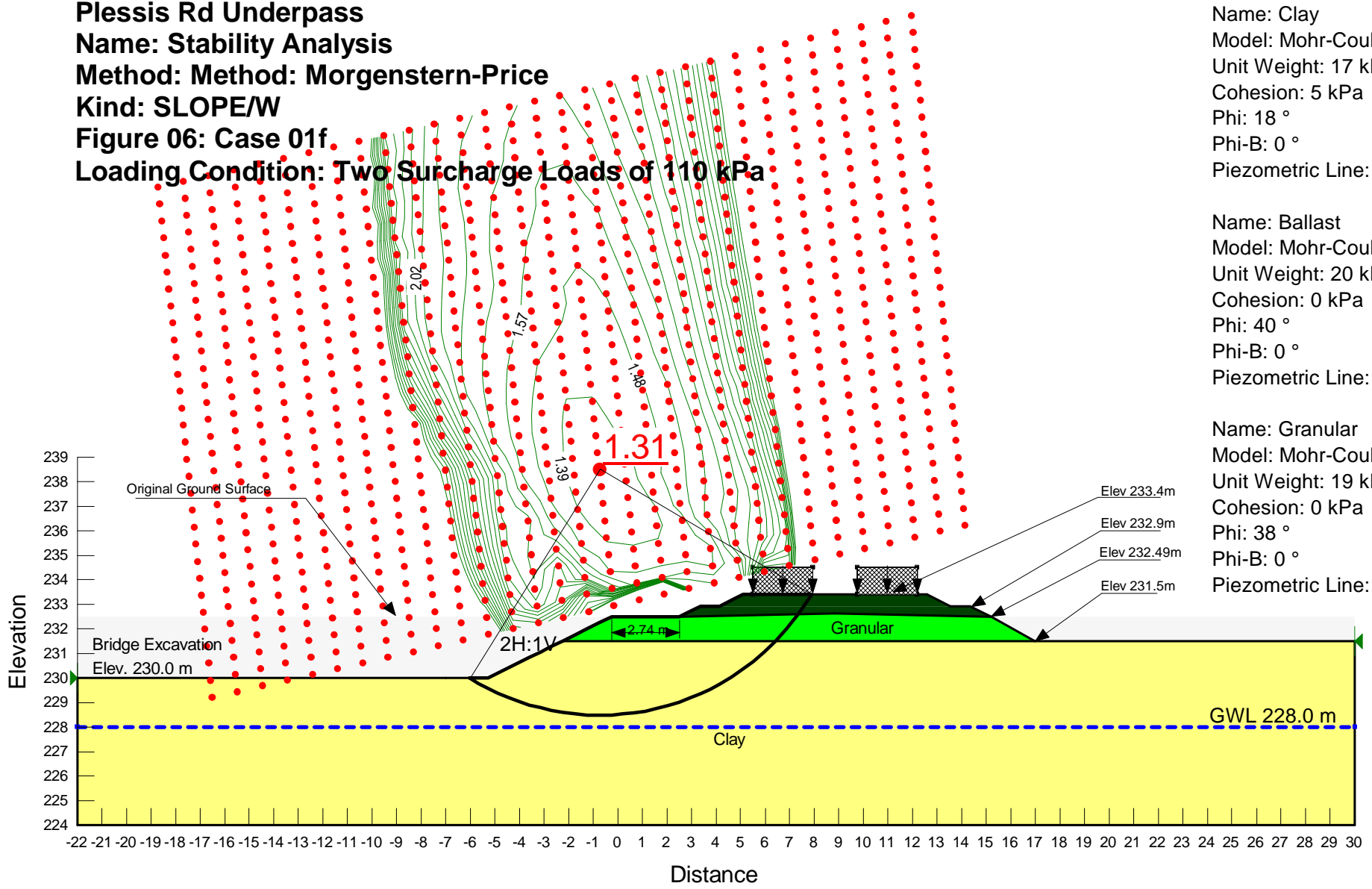


Plessis Rd Underpass
Name: Stability Analysis
Method: Method: Morgenstern-Price
Kind: SLOPE/W
Figure 06: Case 01f
Loading Condition: Two Surcharge Loads of 110 kPa

Name: Clay
 Model: Mohr-Coulomb
 Unit Weight: 17 kN/m³
 Cohesion: 5 kPa
 Phi: 18 °
 Phi-B: 0 °
 Piezometric Line: 1

Name: Ballast
 Model: Mohr-Coulomb
 Unit Weight: 20 kN/m³
 Cohesion: 0 kPa
 Phi: 40 °
 Phi-B: 0 °
 Piezometric Line: 1

Name: Granular
 Model: Mohr-Coulomb
 Unit Weight: 19 kN/m³
 Cohesion: 0 kPa
 Phi: 38 °
 Phi-B: 0 °
 Piezometric Line: 1



Elev 233.4m
 Elev 232.9m
 Elev 232.49m
 Elev 231.5m

GWL 228.0 m

Distance

Plessis Rd Underpass

Name: Roadside Excavation and Embankment Loading

Kind: SIGMA/W

Method: Load/Deformation

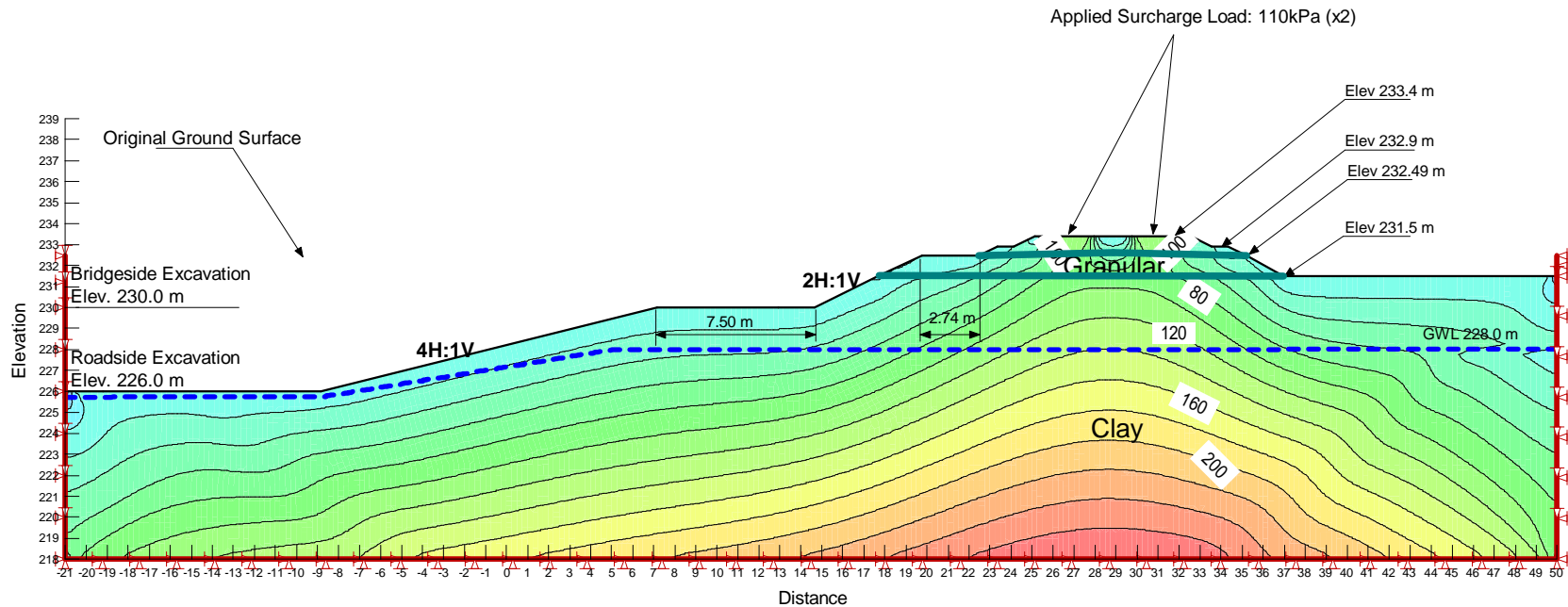
Loading Condition: Surcharge loads of 110 kPa on each Track

Figure 07: Case 02a

Name: Clay
 Model: Linear Elastic
 Effective Young's Modulus (E'): 6000 kPa
 Poisson's Ratio: 0.4
 Insitu Ko: 0.66666667
 Unit Weight: 17 kN/m³

Name: Ballast
 Model: Linear Elastic
 Effective Young's Modulus (E'): 120000 kPa
 Poisson's Ratio: 0.25
 Insitu Ko: 0.33333333
 Unit Weight: 20 kN/m³

Name: Granular
 Model: Linear Elastic
 Effective Young's Modulus (E'): 100000 kPa
 Poisson's Ratio: 0.334
 Insitu Ko: 0.5015015
 Unit Weight: 19 kN/m³



Plessis Rd Underpass

Name: Roadside Excavation Stability Analysis

Kind: SLOPE/W

Method: SIGMA/W Stress

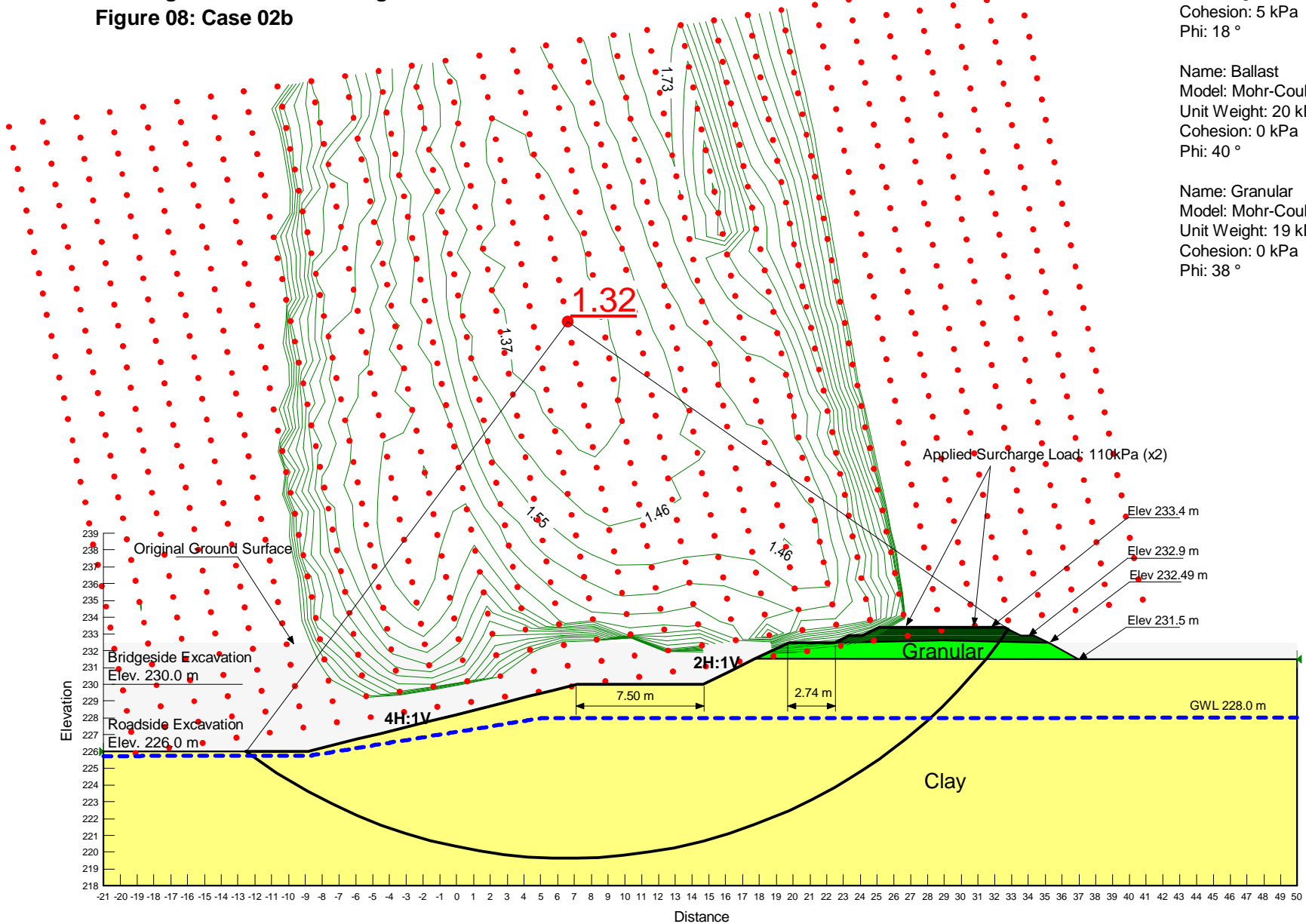
Loading Condition: Surcharge loads of 110 kPa on each Track

Figure 08: Case 02b

Name: Clay
Model: Mohr-Coulomb
Unit Weight: 17.5 kN/m³
Cohesion: 5 kPa
Phi: 18 °

Name: Ballast
Model: Mohr-Coulomb
Unit Weight: 20 kN/m³
Cohesion: 0 kPa
Phi: 40 °

Name: Granular
Model: Mohr-Coulomb
Unit Weight: 19 kN/m³
Cohesion: 0 kPa
Phi: 38 °



Plessis Rd Underpass

Name: Stability Analysis

Kind: SLOPE/W

Method: Morgenstern-Price

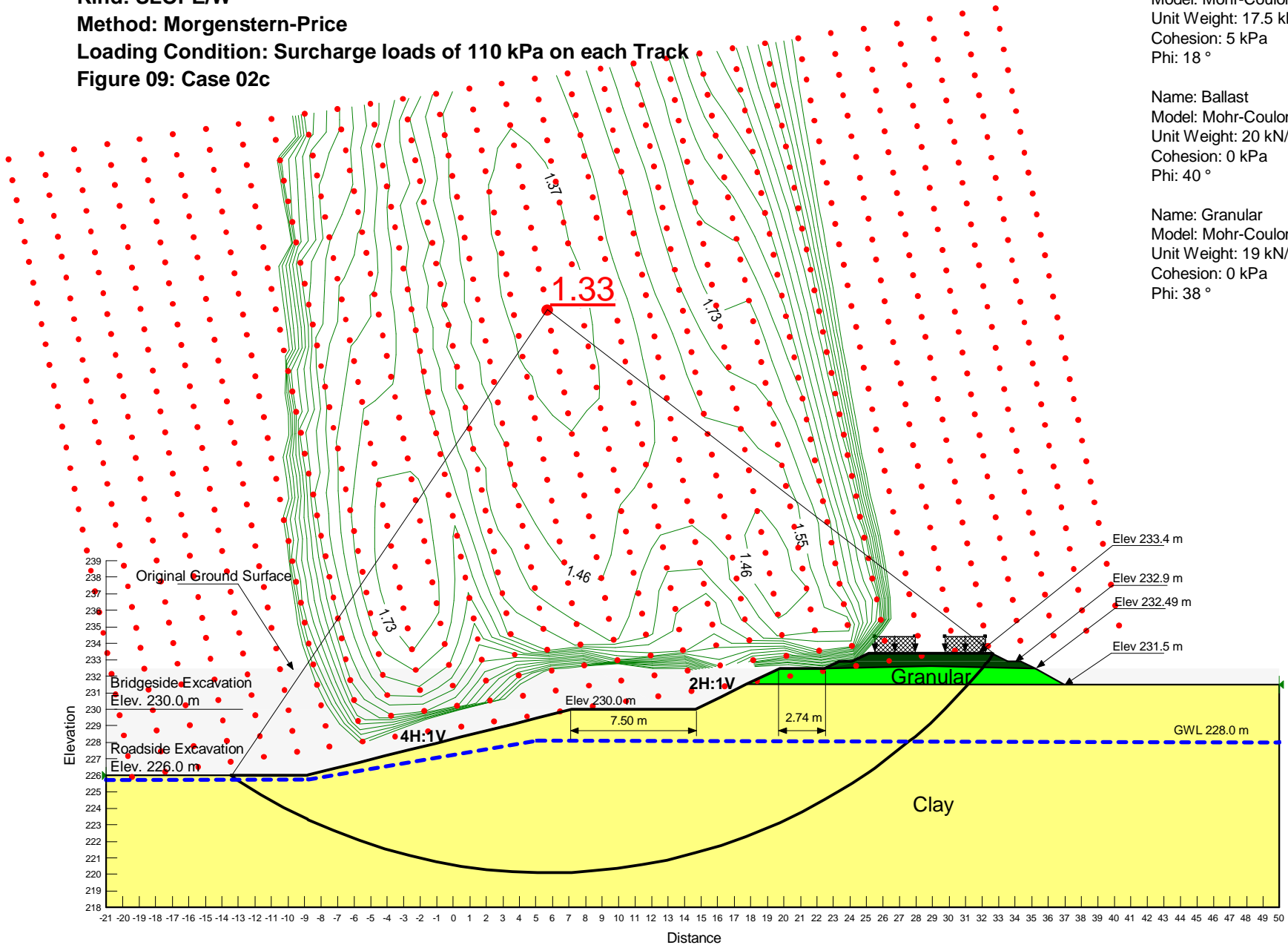
Loading Condition: Surcharge loads of 110 kPa on each Track

Figure 09: Case 02c

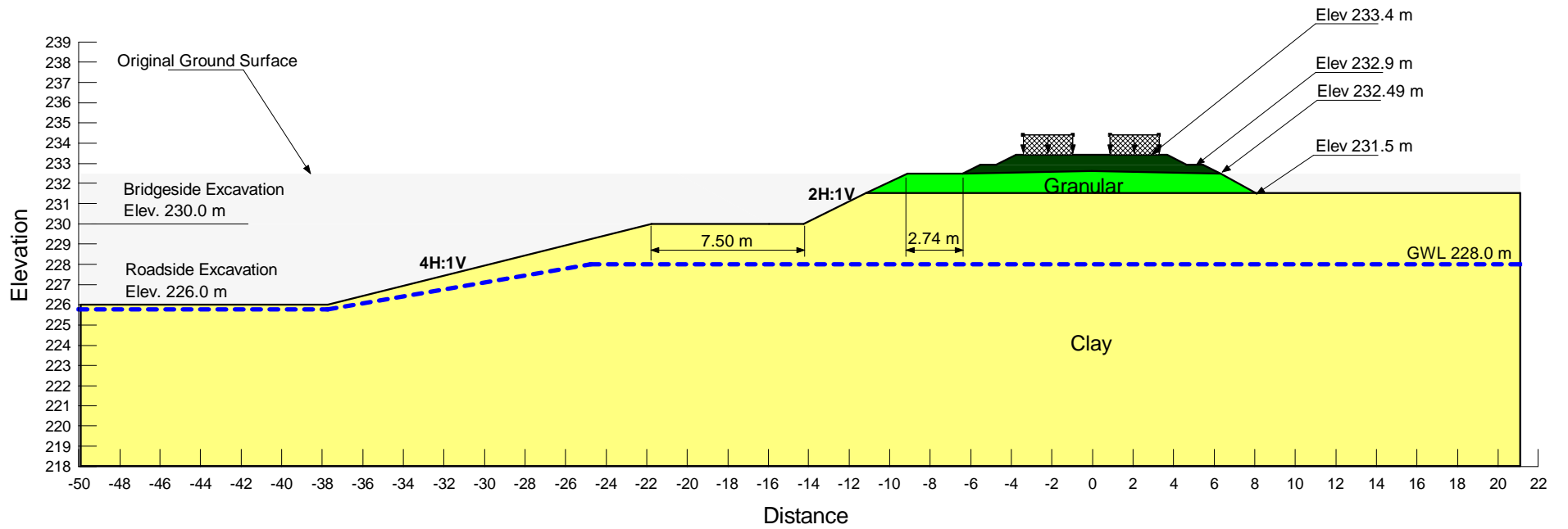
Name: Clay
 Model: Mohr-Coulomb
 Unit Weight: 17.5 kN/m³
 Cohesion: 5 kPa
 Phi: 18 °

Name: Ballast
 Model: Mohr-Coulomb
 Unit Weight: 20 kN/m³
 Cohesion: 0 kPa
 Phi: 40 °

Name: Granular
 Model: Mohr-Coulomb
 Unit Weight: 19 kN/m³
 Cohesion: 0 kPa
 Phi: 38 °



Plessis Rd Underpass
Name: Stability Analysis
Figure 10: Geometry for Case 02



Plessis Rd Underpass

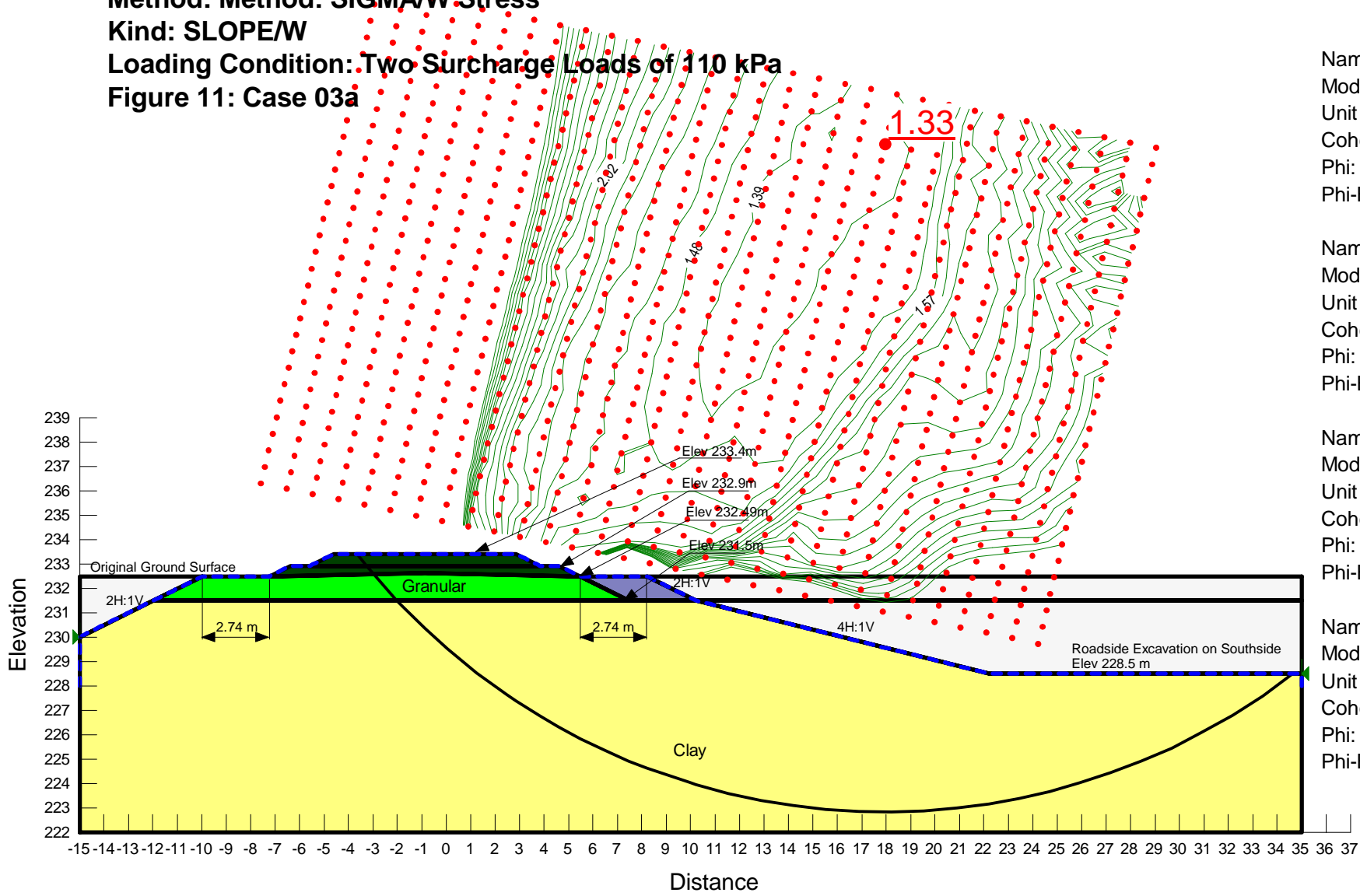
Name: Roadside Excavation Stability Analysis

Method: Method: SIGMA/W Stress

Kind: SLOPE/W

Loading Condition: Two Surcharge Loads of 110 kPa

Figure 11: Case 03a



Name: Clay
Model: Mohr-Coulomb
Unit Weight: 17 kN/m³
Cohesion: 5 kPa
Phi: 18 °
Phi-B: 0 °

Name: Ballast
Model: Mohr-Coulomb
Unit Weight: 20 kN/m³
Cohesion: 0 kPa
Phi: 40 °
Phi-B: 0 °

Name: Granular
Model: Mohr-Coulomb
Unit Weight: 19 kN/m³
Cohesion: 0 kPa
Phi: 38 °
Phi-B: 0 °

Name: Clay Fill
Model: Mohr-Coulomb
Unit Weight: 17 kN/m³
Cohesion: 3 kPa
Phi: 15 °
Phi-B: 0 °

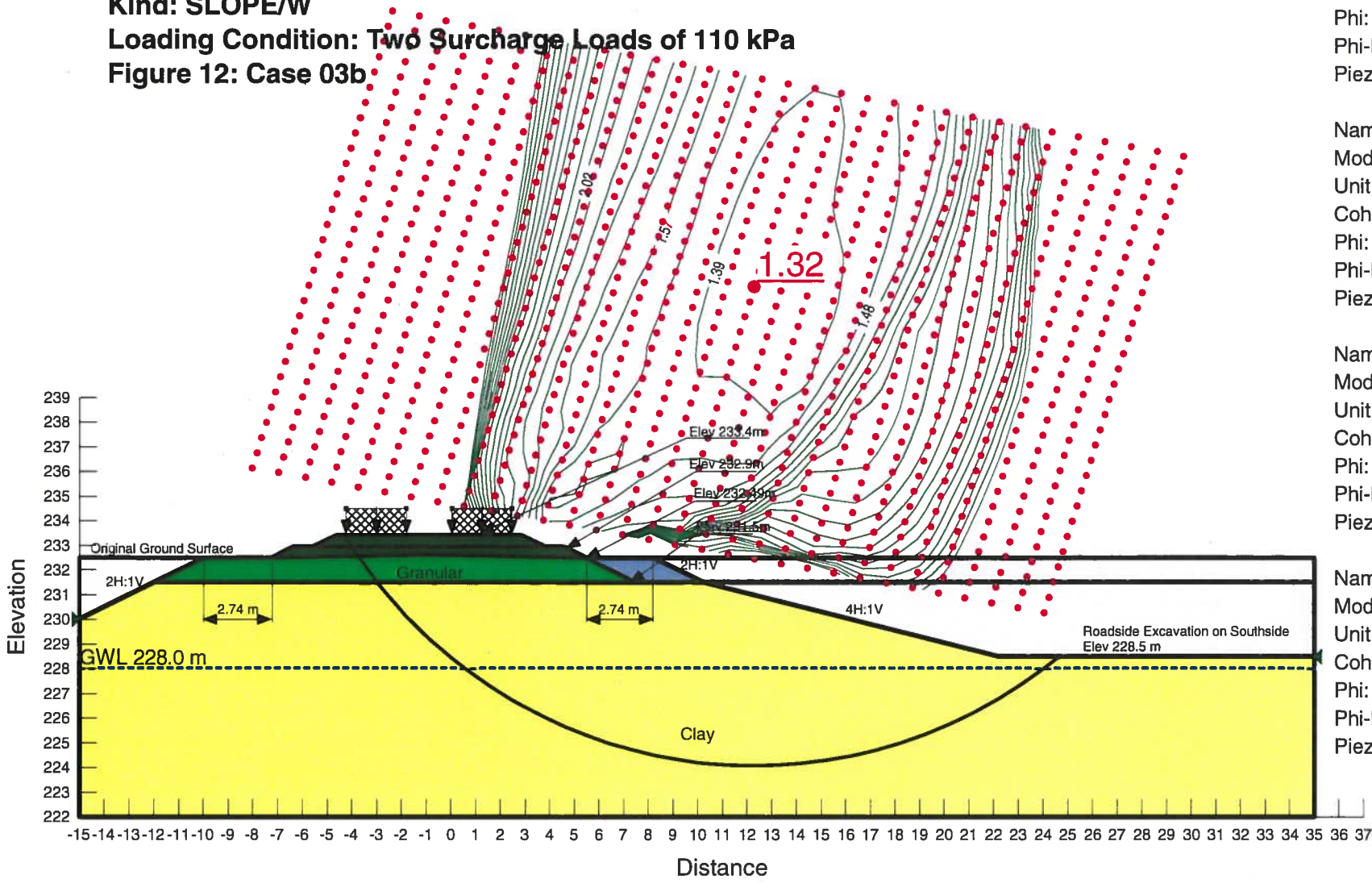
Plessis Rd Underpass
Name: Stability Analysis - Roadside Excavation on Southside
Method: Method: Morgenstern-Price
Kind: SLOPE/W
Loading Condition: Two Surcharge Loads of 110 kPa
Figure 12: Case 03b

Name: Clay
 Model: Mohr-Coulomb
 Unit Weight: 17 kN/m³
 Cohesion: 5 kPa
 Phi: 18 °
 Phi-B: 0 °
 Piezometric Line: 1

Name: Ballast
 Model: Mohr-Coulomb
 Unit Weight: 20 kN/m³
 Cohesion: 0 kPa
 Phi: 40 °
 Phi-B: 0 °
 Piezometric Line: 1

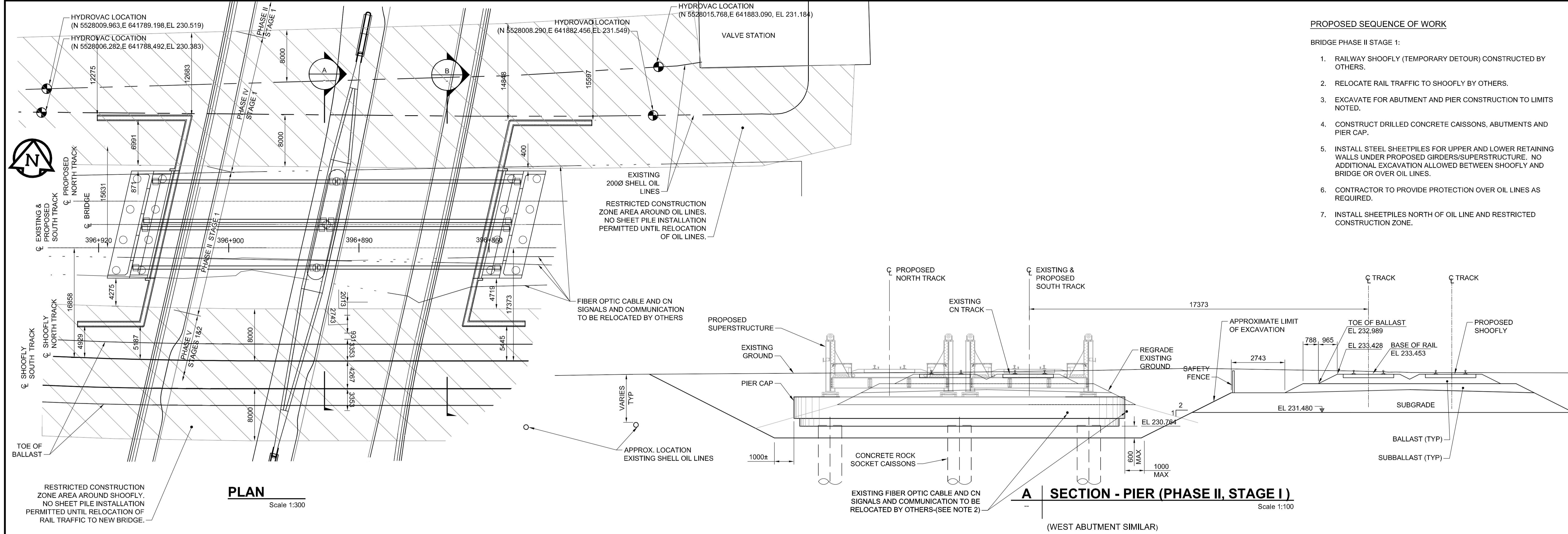
Name: Granular
 Model: Mohr-Coulomb
 Unit Weight: 19 kN/m³
 Cohesion: 0 kPa
 Phi: 38 °
 Phi-B: 0 °
 Piezometric Line: 1

Name: Clay Fill
 Model: Mohr-Coulomb
 Unit Weight: 17 kN/m³
 Cohesion: 3 kPa
 Phi: 15 °
 Phi-B: 0 °
 Piezometric Line: 1



Elevation

Distance

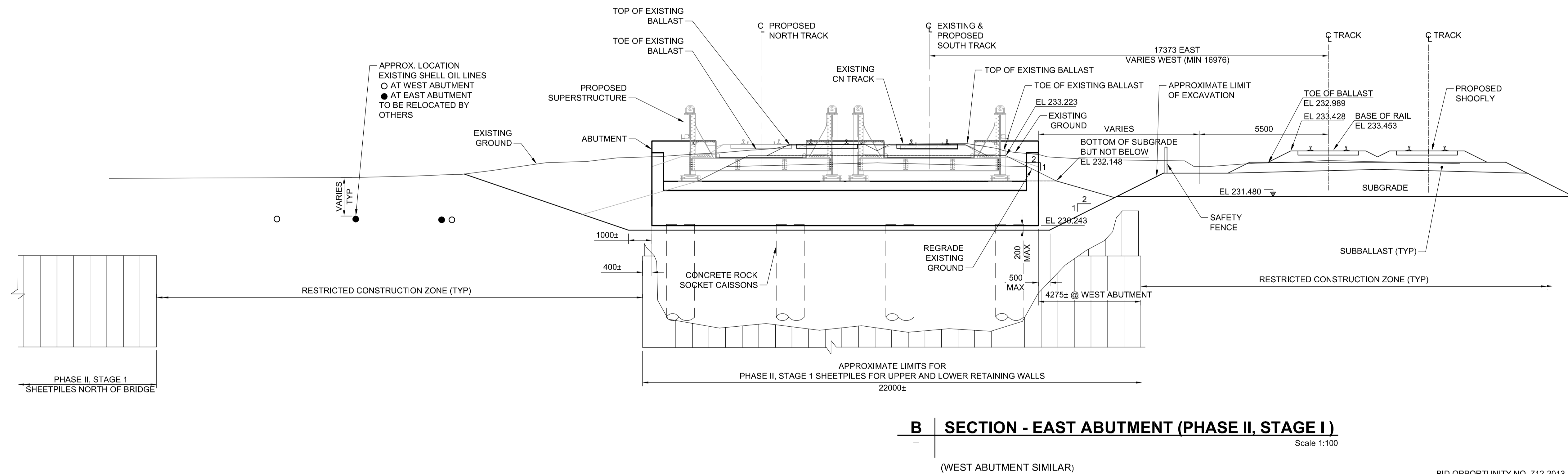


PROPOSED SEQUENCE OF WORK

- BRIDGE PHASE II STAGE 1:
1. RAILWAY SHOOFLY (TEMPORARY DETOUR) CONSTRUCTED BY OTHERS.
 2. RELOCATE RAIL TRAFFIC TO SHOOFLY BY OTHERS.
 3. EXCAVATE FOR ABUTMENT AND PIER CONSTRUCTION TO LIMITS NOTED.
 4. CONSTRUCT DRILLED CONCRETE CAISSONS, ABUTMENTS AND PIER CAP.
 5. INSTALL STEEL SHEETPILES FOR UPPER AND LOWER RETAINING WALLS UNDER PROPOSED GIRDERS/SUPERSTRUCTURE. NO ADDITIONAL EXCAVATION ALLOWED BETWEEN SHOOFLY AND BRIDGE OR OVER OIL LINES.
 6. CONTRACTOR TO PROVIDE PROTECTION OVER OIL LINES AS REQUIRED.
 7. INSTALL SHEETPILES NORTH OF OIL LINE AND RESTRICTED CONSTRUCTION ZONE.

RESTRICTED CONSTRUCTION ZONE AREA AROUND SHOOFLY. NO SHEET PILE INSTALLATION PERMITTED UNTIL RELOCATION OF RAIL TRAFFIC TO NEW BRIDGE.

- NOTES:
1. HYDRO EXCAVATION MAY BE REQUIRED FOR OIL LINES, FIBRE OPTIC CABLE AND CN SIGNALS AND COMMUNICATIONS.
 2. SEE PLAN FOR APPROXIMATE LOCATION OF FIBER OPTIC CABLE AND CN SIGNALS AND COMMUNICATION.
 3. SEE SPECIFICATIONS FOR OVERALL PROJECT PHASES AND STAGES.



LOCATION APPROVED UNDERGROUND STRUCTURES		B.M. ELEV.
SUPV. U/G STRUCTURES COMMITTEE	DATE	
NOTE: LOCATION OF UNDERGROUND STRUCTURES AS SHOWN ARE BASED ON THE BEST INFORMATION AVAILABLE, BUT NO GUARANTEE IS GIVEN THAT ALL EXISTING UTILITIES ARE SHOWN OR THAT THE GIVEN LOCATIONS ARE EXACT. CONFIRMATION OF EXISTENCE AND EXACT LOCATION OF ALL SERVICES MUST BE OBTAINED FROM THE INDIVIDUAL UTILITIES BEFORE PROCEEDING WITH CONSTRUCTION.		
NO.	ISSUED FOR TENDER	DATE
0	ISSUED FOR TENDER	2013/10/15
NO.	REVISIONS	DATE

AECOM		ENGINEER'S SEAL	
DESIGNED BY	FTZS	CHECKED BY	EBL
DRAWN BY	DJH	APPROVED BY	EBL
HOR. SCALE:	AS NOTED	RELEASED FOR CONSTRUCTION BY:	
VERTICAL:	AS NOTED		
DATE	2013-06-04	DATE	

CONSULTANT DRAWING NO. 60273041-01-CS-004	
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THE CITY OF WINNIPEG
PUBLIC WORKS DEPARTMENT

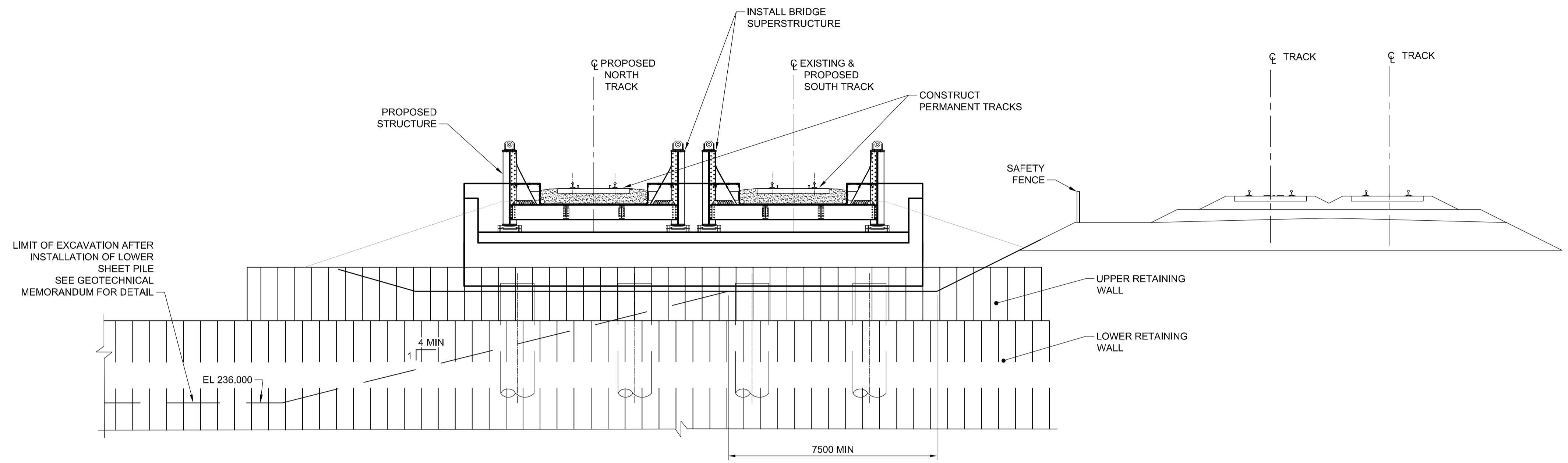
PLESSIS ROAD TWINNING AND GRADE SEPARATION AT CN REDDITT SUBDIVISION CONTRACT 3

CITY DRAWING NUMBER P-3346-2004
SHEET 04 OF 37

BRIDGE STAGING PLAN - SHEET 1

CS-0004

BID OPPORTUNITY NO. 712-2013

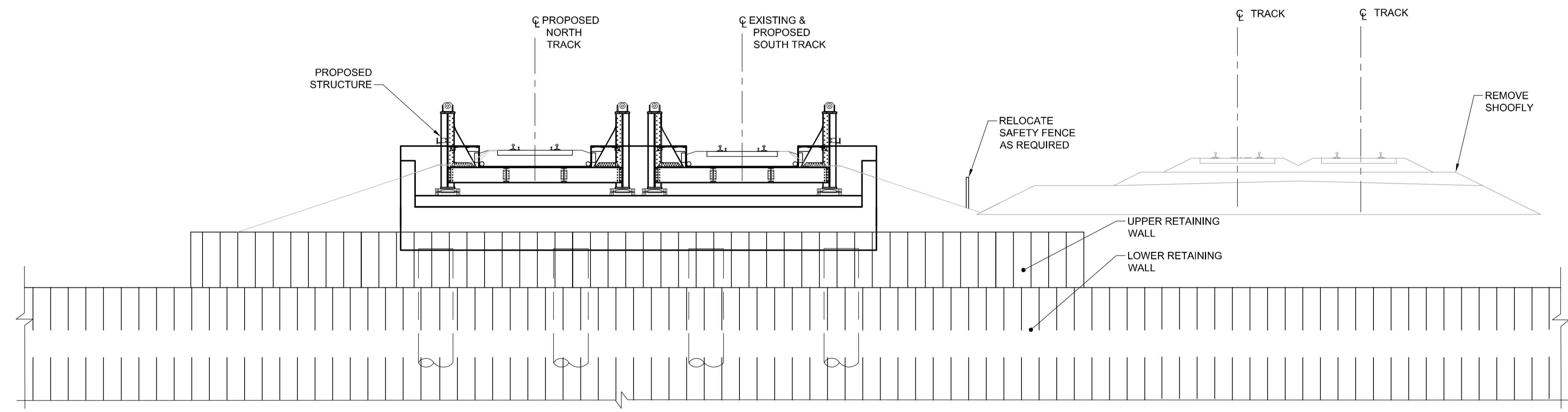


A SECTION - EAST ABUTMENT (PHASE IV, STAGE I)
 CS-0004 Scale 1:100
 (WEST ABUTMENT SIMILAR)

PROPOSED SEQUENCE OF WORK

BRIDGE PHASE IV, STAGE I:

1. INSTALL SUPERSTRUCTURE (BEARINGS, STEEL TPG SPANS, TRAINMAN'S WALKWAY, WATERPROOFING).
2. CONSTRUCT PERMANENT TRACKS OVER BRIDGE AND APPROACHES.
3. RELOCATE RAIL TRAFFIC TO NEW STRUCTURE, PUT MAIN TRACKS BACK INTO SERVICE.
4. RELOCATE FIBRE OPTIC CABLE AND CN SIGNALS AND COMMUNICATION ONTO NEW BRIDGE BY OTHERS.
5. INSTALL SHEET PILES IN RESTRICTED CONSTRUCTION ZONE NORTH OF BRIDGE AFTER OIL LINES RELOCATED BY OTHERS.



A SECTION - EAST ABUTMENT (PHASE V, STAGE I & 2)
 CS-0004 Scale 1:100
 (WEST ABUTMENT SIMILAR)

PROPOSED SEQUENCE OF WORK

BRIDGE PHASE V, STAGE I & 2:

1. REMOVE TEMPORARY RAILWAY SHOOFLY.
2. EXCAVATE BENEATH BRIDGE STRUCTURE.
3. INSTALL STEEL SHEETPILES SOUTH OF BRIDGE STRUCTURE.

APEGM
 Certificate of Authorization
 AECOM Canada Ltd.
 No. 4671 Date: 2013/10/15

LOCATION APPROVED UNDERGROUND STRUCTURES SUPV. U/G STRUCTURES COMMITTEE DATE NOTE: LOCATION OF UNDERGROUND STRUCTURES AS SHOWN ARE BASED ON THE BEST INFORMATION AVAILABLE, BUT NO GUARANTEE IS GIVEN THAT ALL EXISTING UTILITIES ARE SHOWN OR THAT THE GIVEN LOCATIONS ARE EXACT. CONFIRMATION OF EXISTENCE AND EXACT LOCATION OF ALL SERVICES MUST BE OBTAINED FROM THE INDIVIDUAL UTILITIES BEFORE PROCEEDING WITH CONSTRUCTION.	B.M. ELEV.			ENGINEER'S SEAL 	THE CITY OF WINNIPEG PUBLIC WORKS DEPARTMENT		CITY DRAWING NUMBER P-3346-2005
					DESIGNED BY FTZS	CHECKED BY EBL	PLESSIS ROAD TWINNING AND GRADE SEPARATION AT CN REDDITT SUBDIVISION CONTRACT 3
		DRAWN BY DJH	APPROVED BY EBL		BRIDGE STAGING PLAN - SHEET 2		CS-0005
	0 ISSUED FOR TENDER 2013/10/15 KC NO. REVISIONS DATE BY DATE 2013-06-04 DATE	HOR. SCALE: AS NOTED	RELEASED FOR CONSTRUCTION BY:		CONSULTANT DRAWING NO. 60273041-01-CS-005		